



*The 14th Conference on  
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# Creating new multi-domain digital twins of LEDs with an attempt to describe their ageing for predictive maintenance schemes

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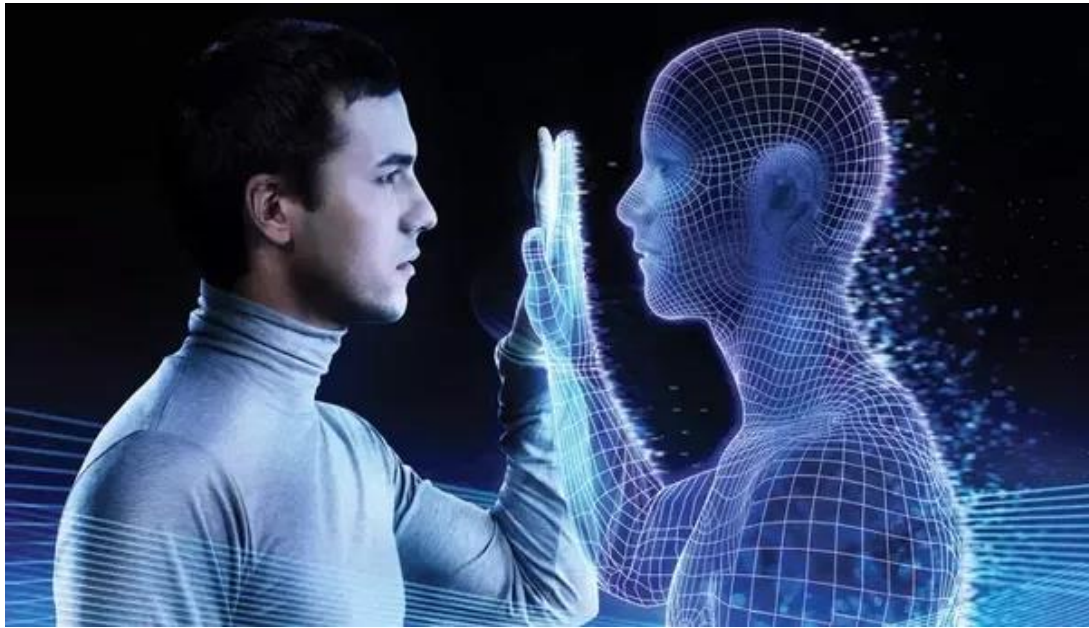
# SIEMENS

<sup>2</sup> Siemens Digital Industry Software  
Simulation and Test Solutions  
Strategy and Innovation, Technology Innovation group

## What are the digital twins (DT-s)?

"**Digital twin** refers to a **digital replica of physical assets, processes and systems** that can be used for various purposes. The digital representation provides both the elements and the dynamics of how an IoT device, equipment, or machine operates and lives throughout its life cycle."

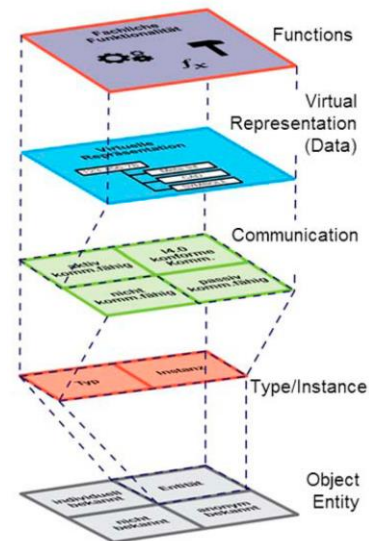
<https://niotek.net/digital-twin/>



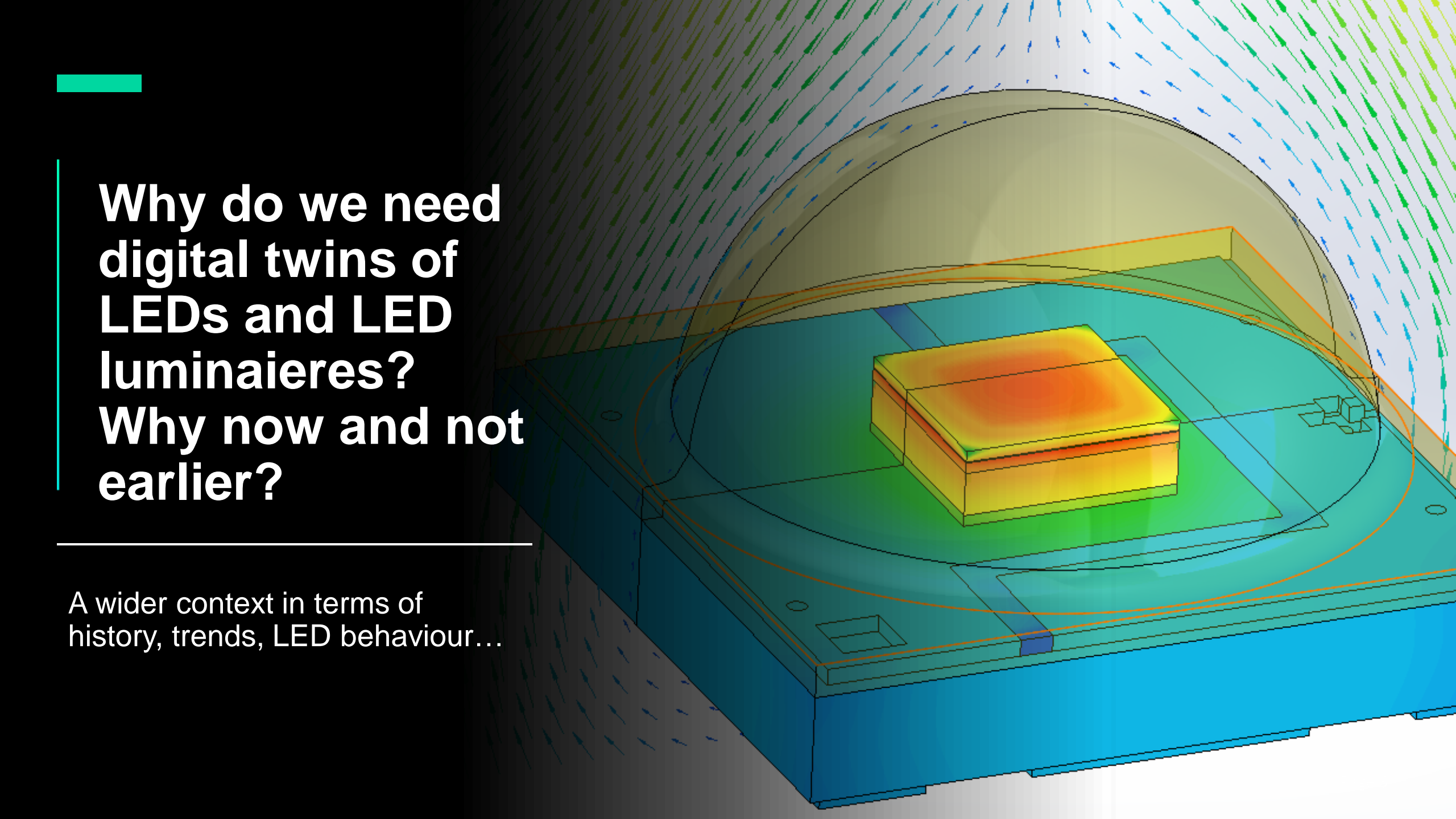
<https://niotek.net/digital-twin/>

With the help digital twins:

- **Product design/development can be speeded up** and development costs can be reduced by avoiding iteration cycles that traditionally involve building and testing physical prototypes → **virtual prototyping**
- Complex optimization
- **During lifetime**, monitoring, diagnostics, prognostics, optimization of operation (performance, utilization) can be achieved by a DT



Schluse, M.; Rossmann, J. From simulation to experimentable digital twins: Simulation-based development and operation of complex technical systems, <https://dx.doi.org/10.1109/SysEng.2016.7753162>



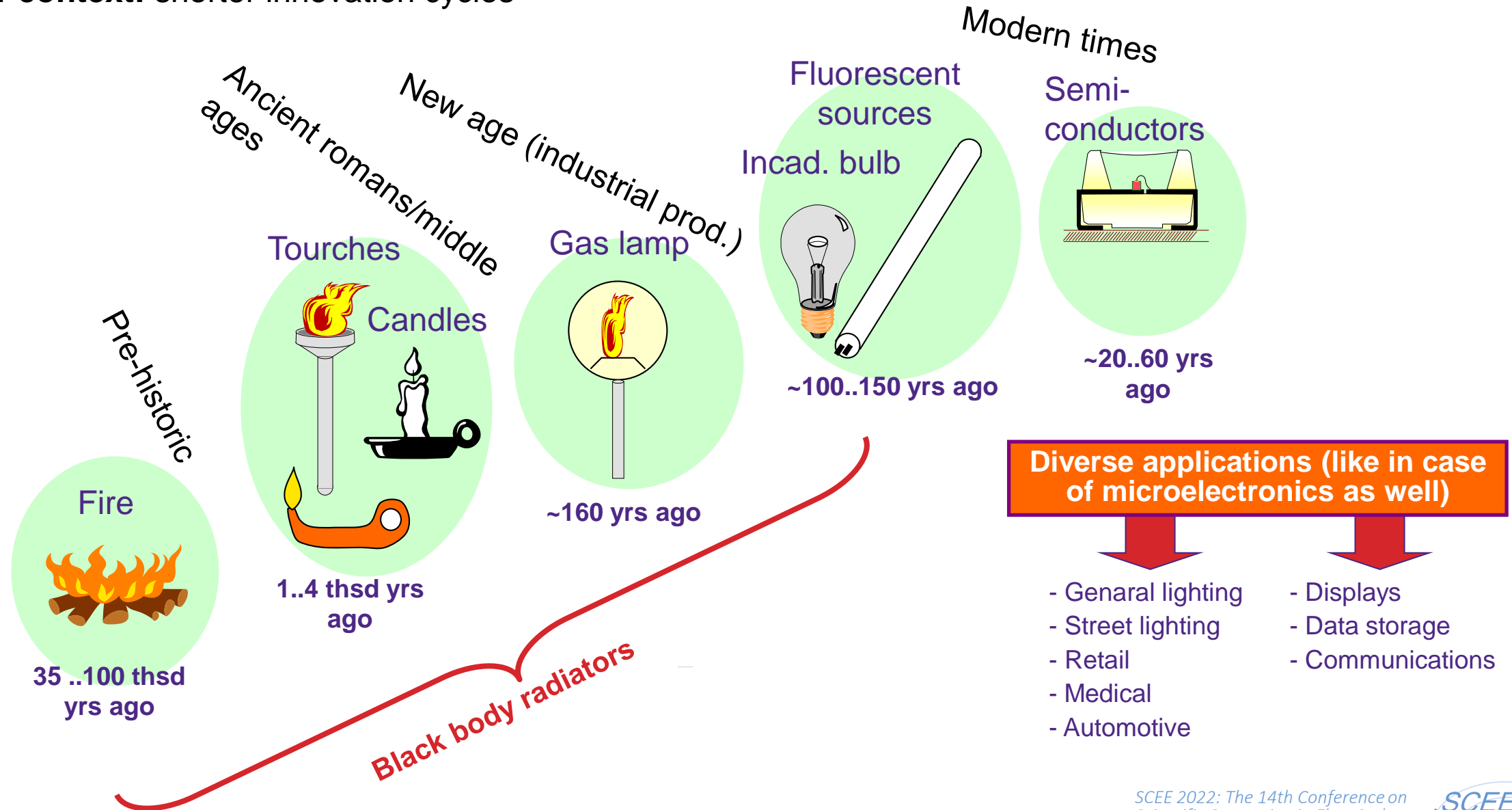
**Why do we need  
digital twins of  
LEDs and LED  
luminaires?  
Why now and not  
earlier?**

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A wider context in terms of  
history, trends, LED behaviour...

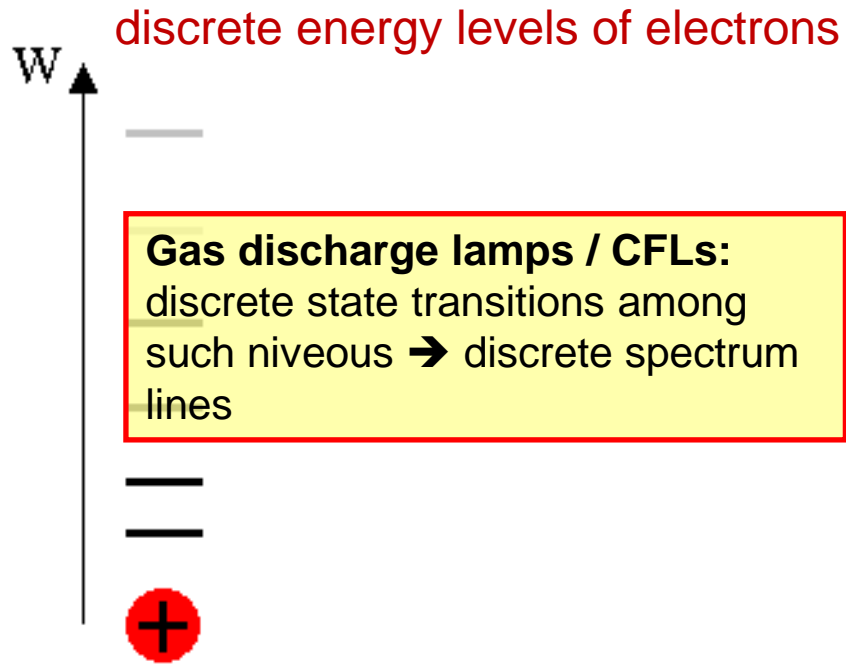
# Why to deal with digital twins of LEDs?

The wider context: shorter innovation cycles



# Why to deal with digital twins of LEDs?

The wider context: **vacuum technology** replaced by **semiconductor technology** and electronics assembly



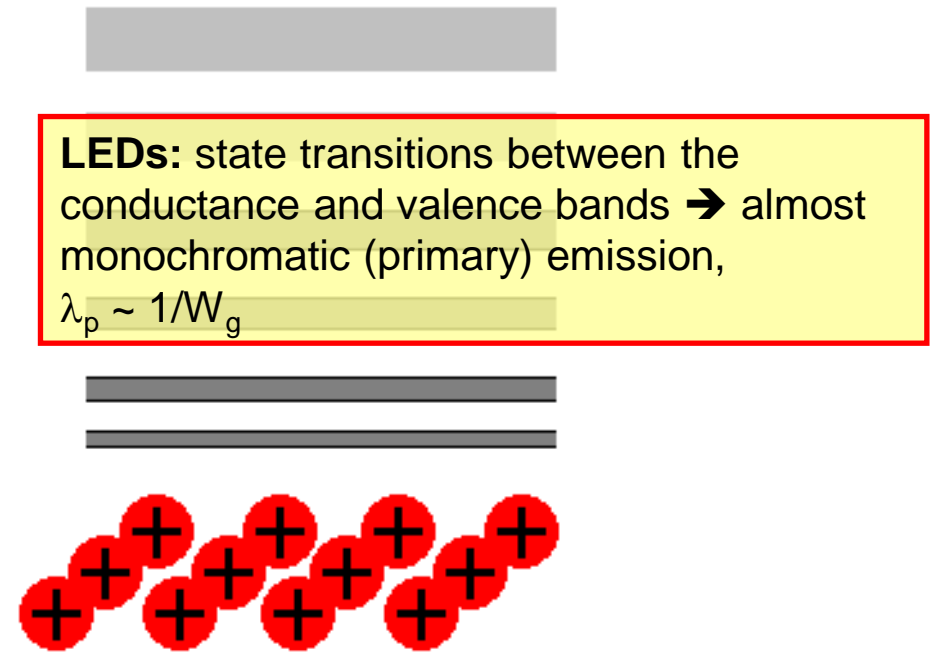
**classical light sources**

electron tubes

**vacuum technology**

**Heating needed / helps the operation**

in the semiconductor crystal, the single niveous split into bands



**solid-state light sources**

semiconductor diodes / transistors

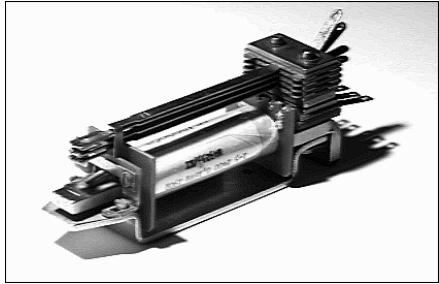
**semiconductor technology**

**Cooling is required for the proper operation**

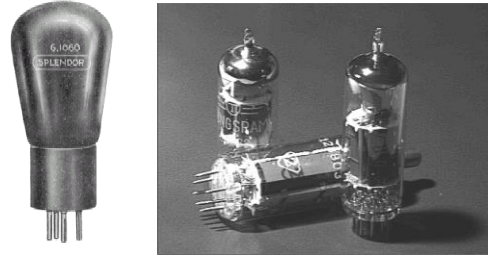
# Why to deal with digital twins of LEDs?

**The wider context:** electric lighting has a similar development path as electronics, catching up in speed...

1837 Morse: telegraph (electro mechanical)

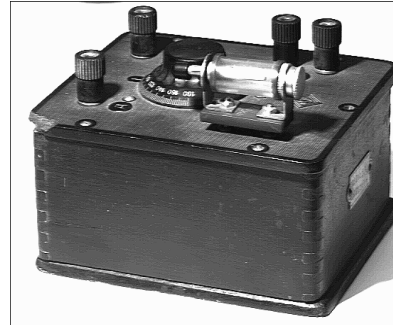


Electron tubes (rectifiers, amplifiers)

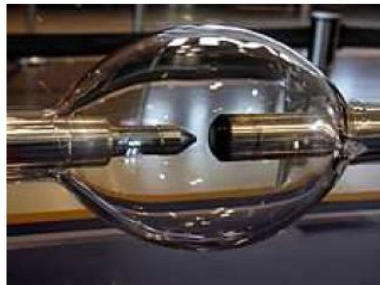
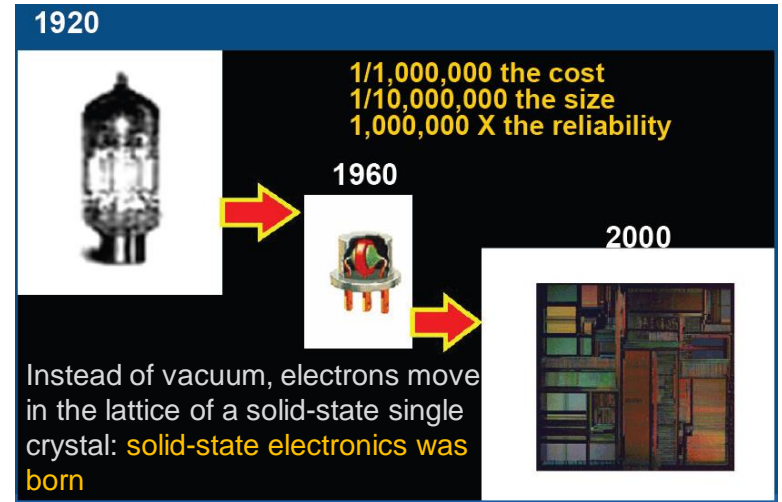


Electron devices

All electric radio



Based on electron devices electronics was born



Arc lamp: 1841



Edisons light bulb: 1879



Fluorescent lamp: 1926



First LEDs (red): 1962

1989: GaN homo-junction LED  
1993: High efficiency blue LED  
2014: Nobel Prize for Physics

The high-efficiency "L-prize" bulb, August 2011 (60W incandescent replacement)



LED lamps: ~1998



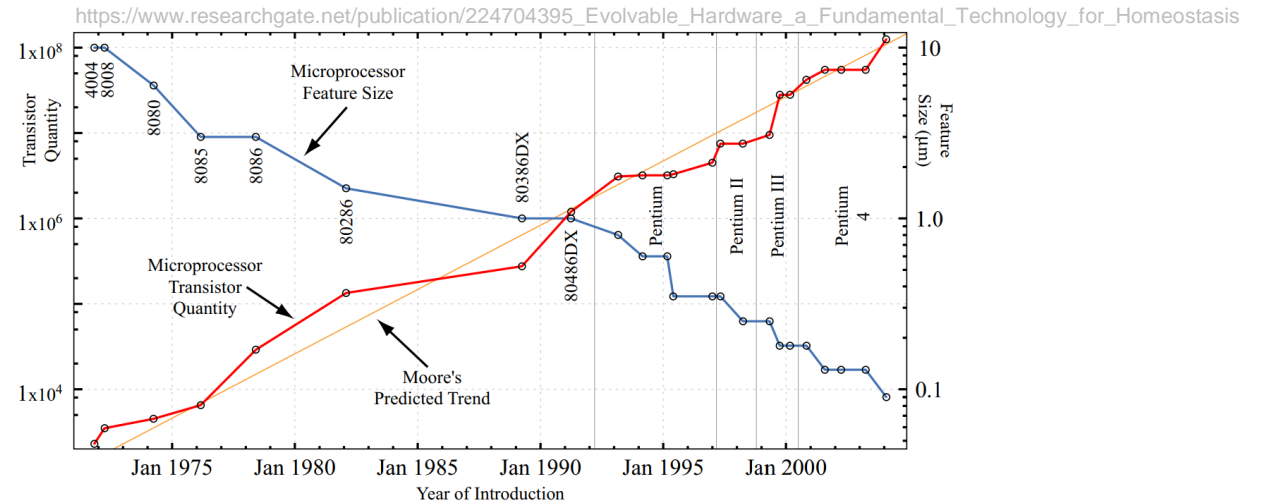
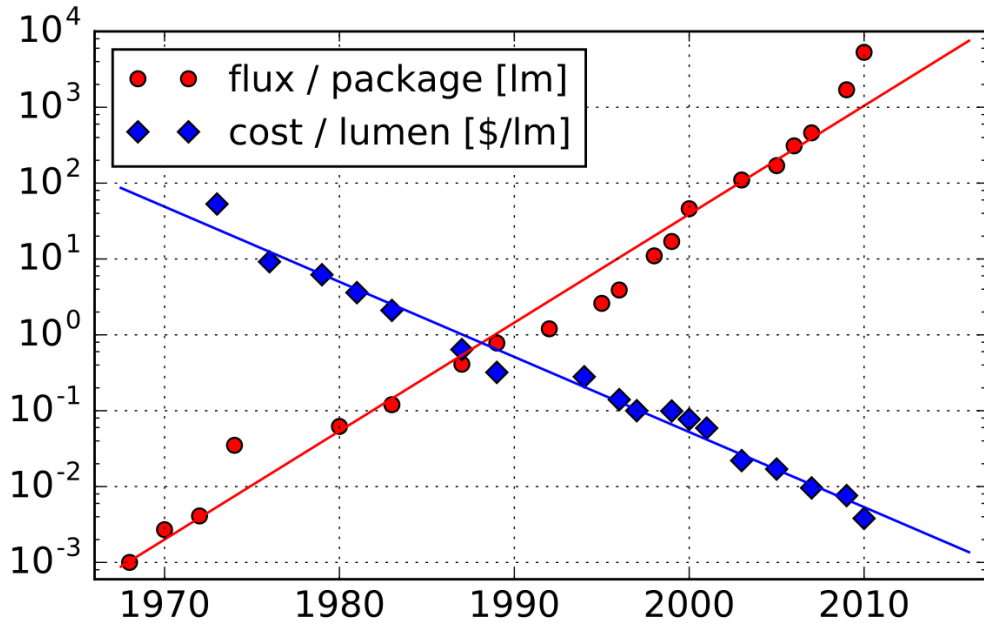
Philips' 70W HPS replacement, 2018

Philips' Hue bulbs with integrated smart control + communications, October 2012, for iPhone



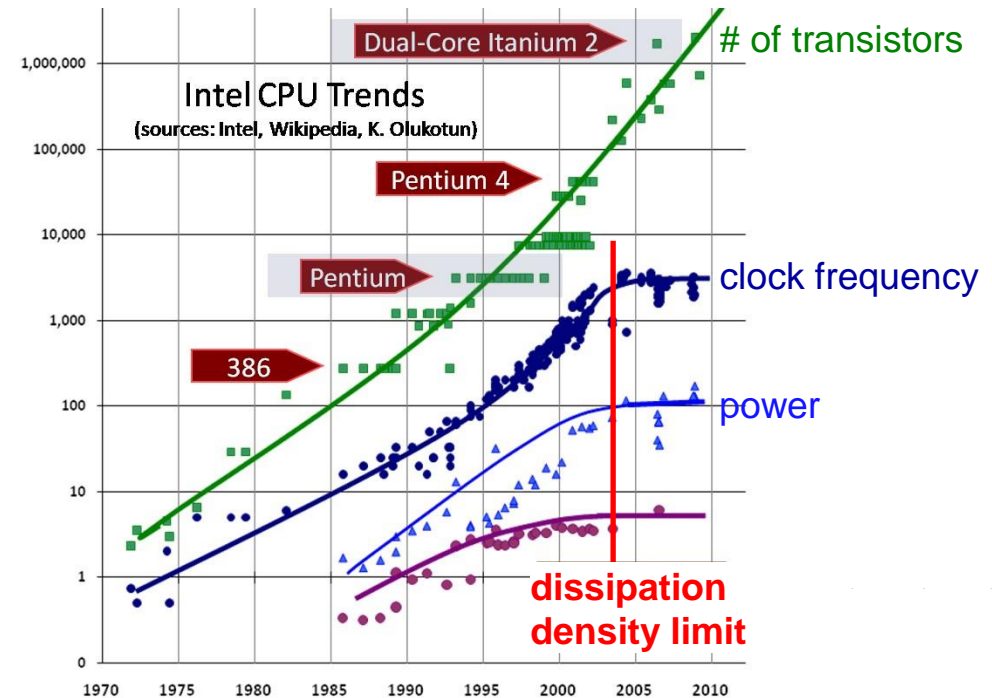
# Why to deal with digital twins of LEDs?

The wider context: solid-state lighting has similar development trends as microelectronics:  
**Haitz's law** is the Moore's law of SSL



There are fundamental limits of development...

**An important practical limit** though, both in microelectronics and SSL, **is the manageable heat dissipation density...**



# The (solid-state) lighting industry became a special part of the electronics industry

- **Success in LEDification → classical light sources disappear** (as well as their manufacturers)

- Selling incandescent bulbs banned in the EU, CFLs begin to phase out now
- LED retrofit HPS replacement on the market

On top of the above, **today's high energy prices** (gas, electricity) represent further **drives for rapid changes**

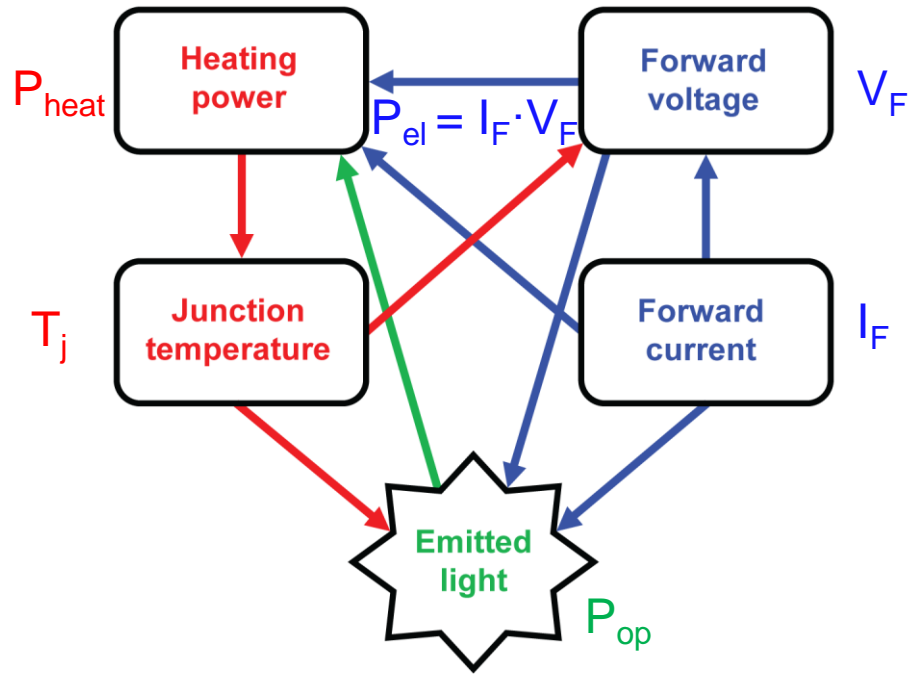
- Glass-based solutions are becoming too expensive to produce due to the high energy need of manufacturing (glass factories for bulb manufacturing are in trouble). *Is manufacturing of filament LED bulbs in danger?*
  - Energy cost reduction is getting even more urgent than a few years ago...
- **LEDs are semiconductor devices**
    - Characteristics of the semiconductor industry apply..., e.g. computerized, simulation-based design: wide use of TCAD and EDA tools
  - **LED modules are produced by electronics assembly processes**
    - PCB design and manufacturing
  - **LED luminaires are complex electronic systems** (classical ones were just lamp fixtures & holders of optics)
    - LED luminaires include delicate electronics (LED drivers, smart controls, diagnostics, communications)
    - LEDs need proper cooling, thus, luminaires have to provide delicate thermal management solutions as well

Until recently, using EDA tools has not been a common practice at luminaire makers, electrical, mechanical and optical design teams are de-coupled

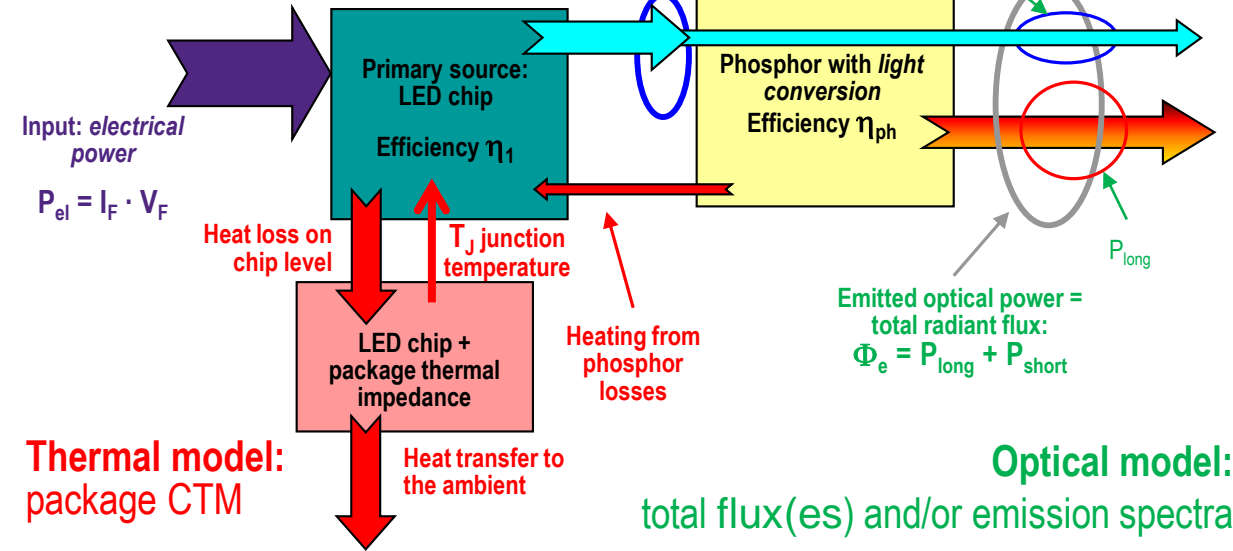


# Why to deal with digital twins of LEDs?

The wider context: complex operation in 3 closely coupled operating domains...



**Electrical model:**  
LED pn junction I-V characteristic



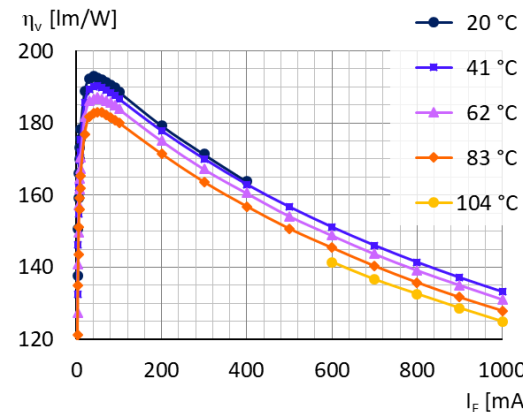
**Thermal model:**  
package CTM

**Optical model:**  
total flux(es) and/or emission spectra

LEDs' electric operating point determines its light output but also gives rise to self-heating.

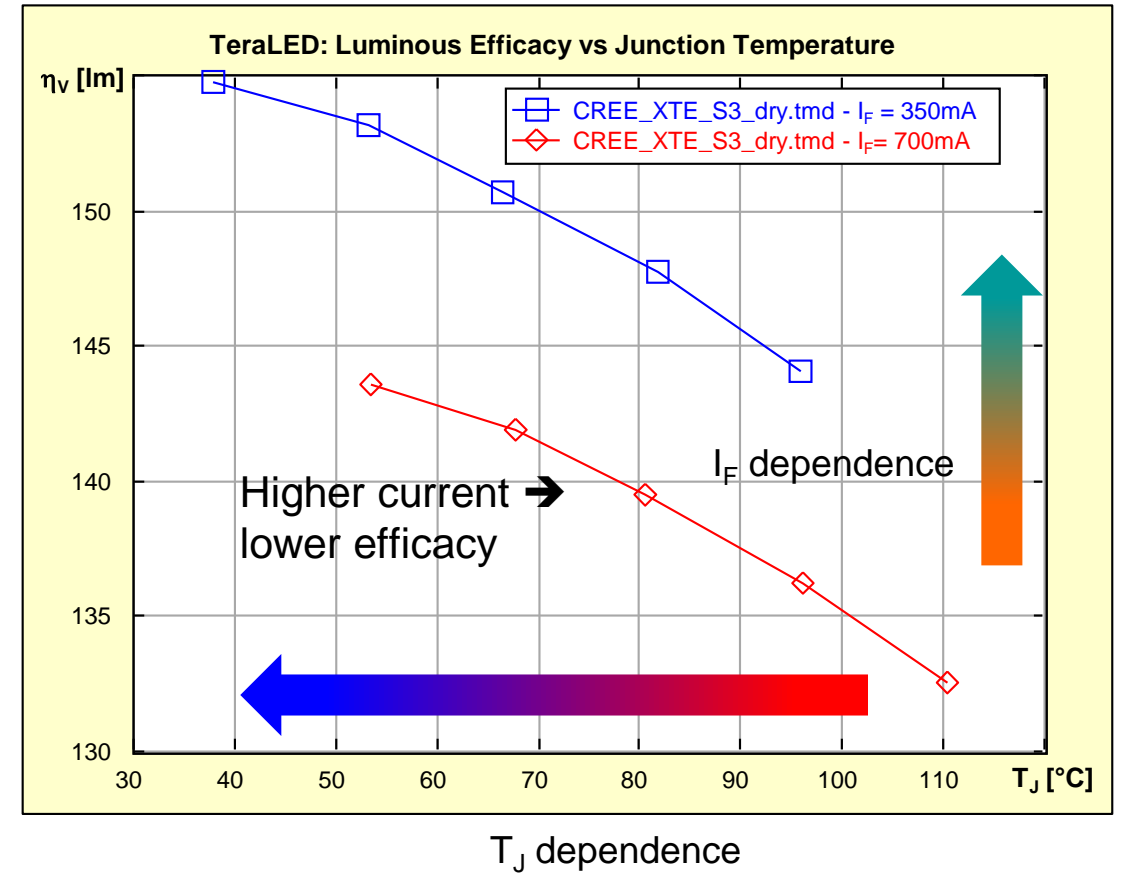
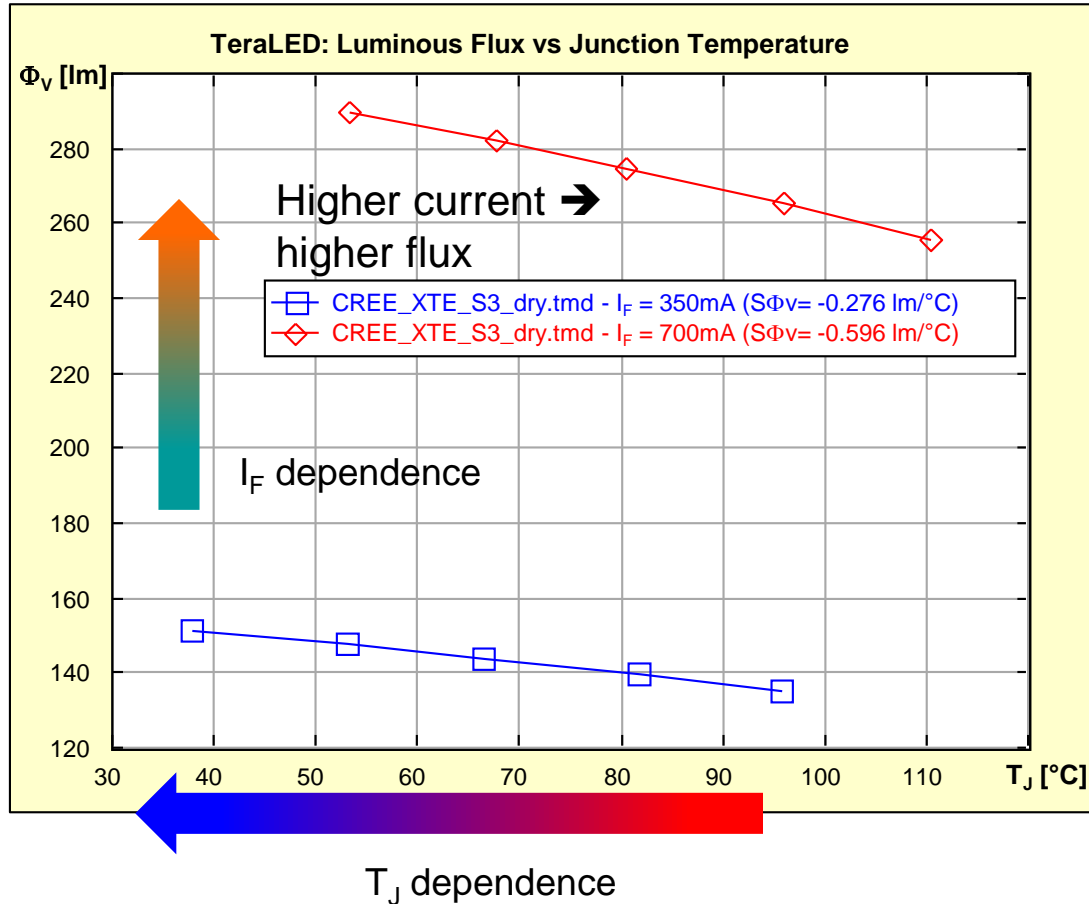
$$P_{opt} = P_{el} - P_{heat}$$

More heat results in higher junction temperature  
Higher junction temperature results in reduction of efficiency and shorter lifetime...



# Why to deal with digital twins of LEDs?

The wider context: LED operating point has to be optimized that needs careful design based on simulations



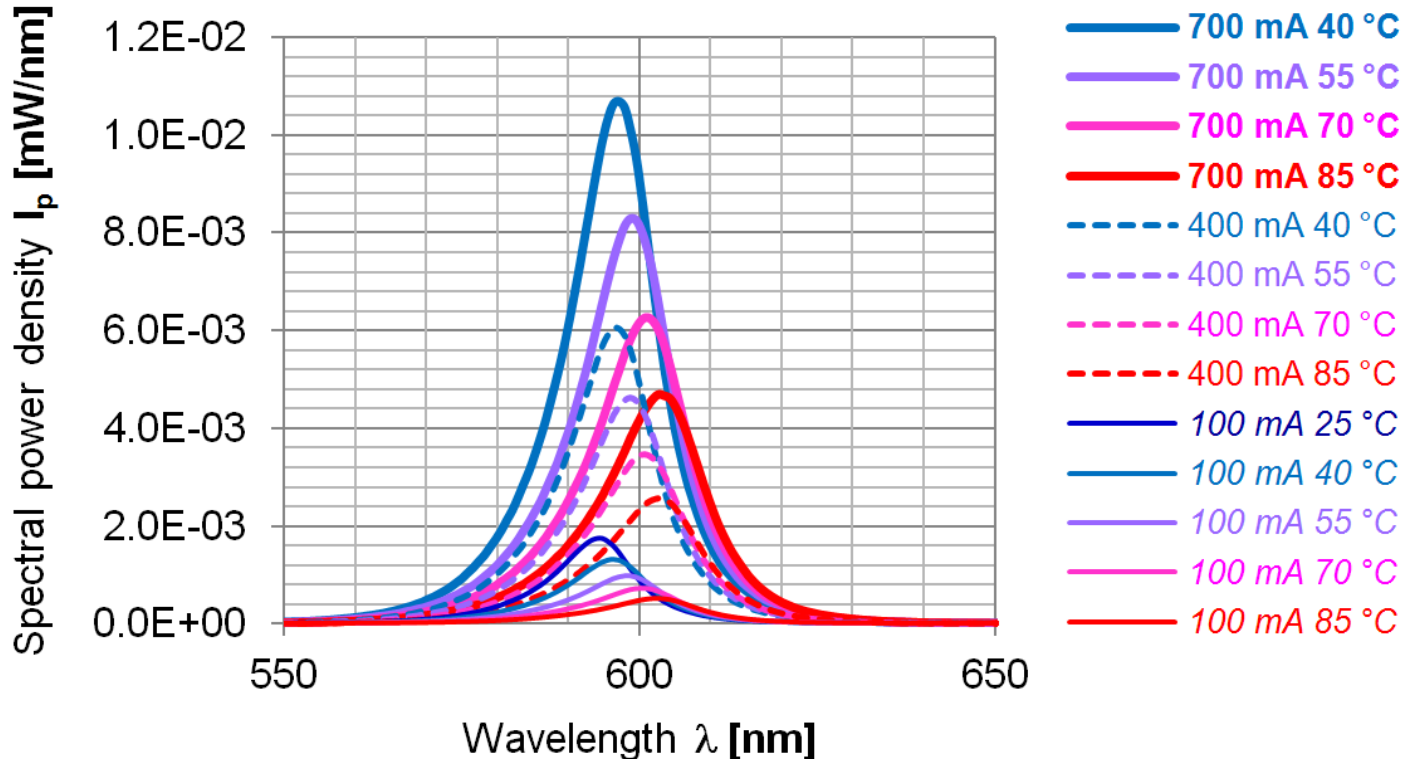
At higher current more light is generated but less efficiently. How to find good trade-offs?

# Why to deal with digital twins of LEDs?

**The wider context:** some other aspects of the LEDs' complex operation  
Peak wavelength & intensity vs.  $T_j$  for a colour LED

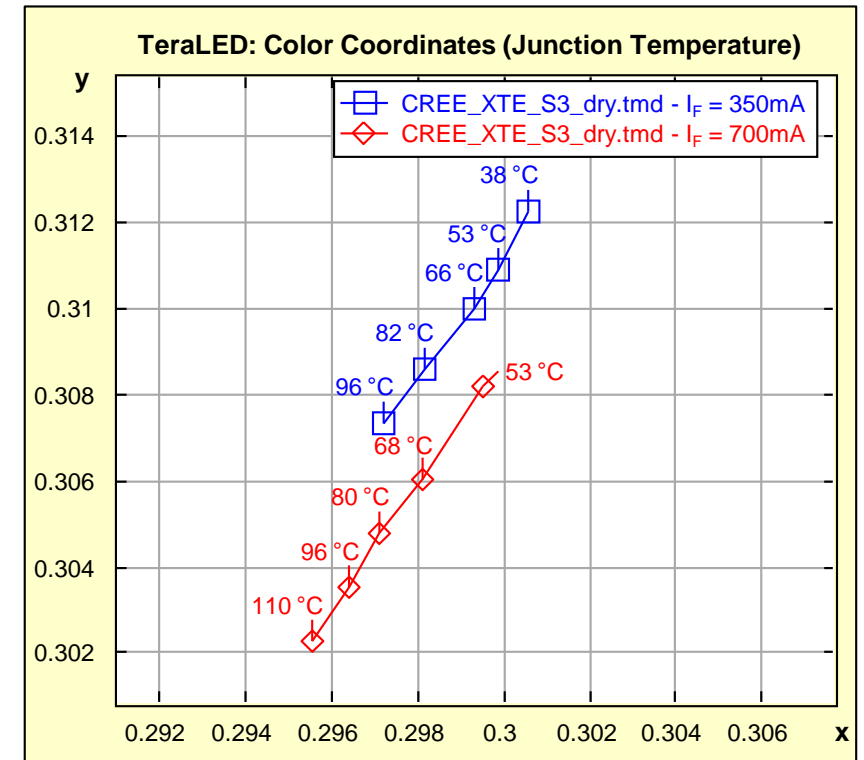
Peak wavelength shifts, intensity diminishes

**SPDs of an amber LED measured at different junction temperatures**



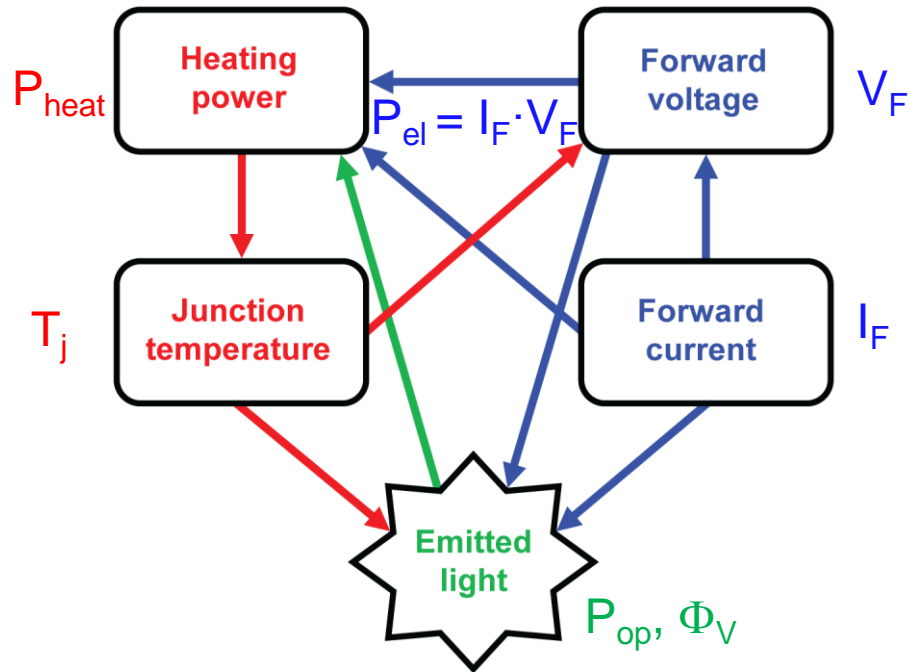
Colour point shifts of a white LED

(CIE 1931 2° observer)



# Why to deal with digital twins of LEDs?

LEDs need to be properly modelled for the usual EDA software tools



Light output parameters of LEDs depend on *everything*

Their interdependence should be **modelled** for **lighting designers**  
“**Hot lumens**” calculations

- electrical
- thermal &
- optical

properties calculated simultaneously → **multi-domain approach**

**Chip level:** multi-domain LED model (electrical, optical, thermal)

- Calculation of the diode characteristics
- Calculation of the emitted flux (optical power, luminous flux)
  - Effect of lens and phosphor lumped into the model
- Calculation of the temperature dependence of the above

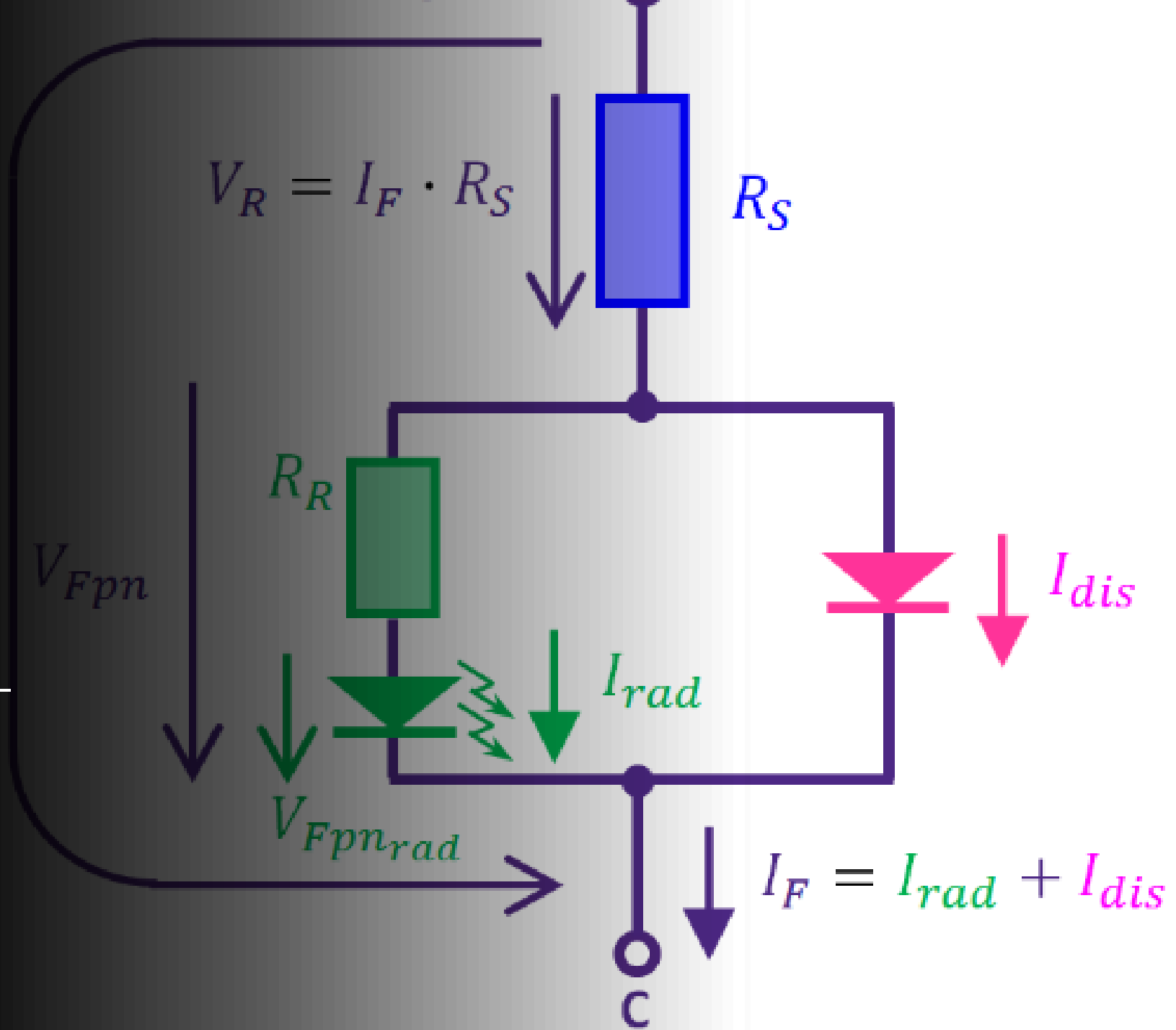
**Package level:** compact thermal model of the heat-flow path

- Dynamic model, with a complexity corresponding to the mechanical structure of the package

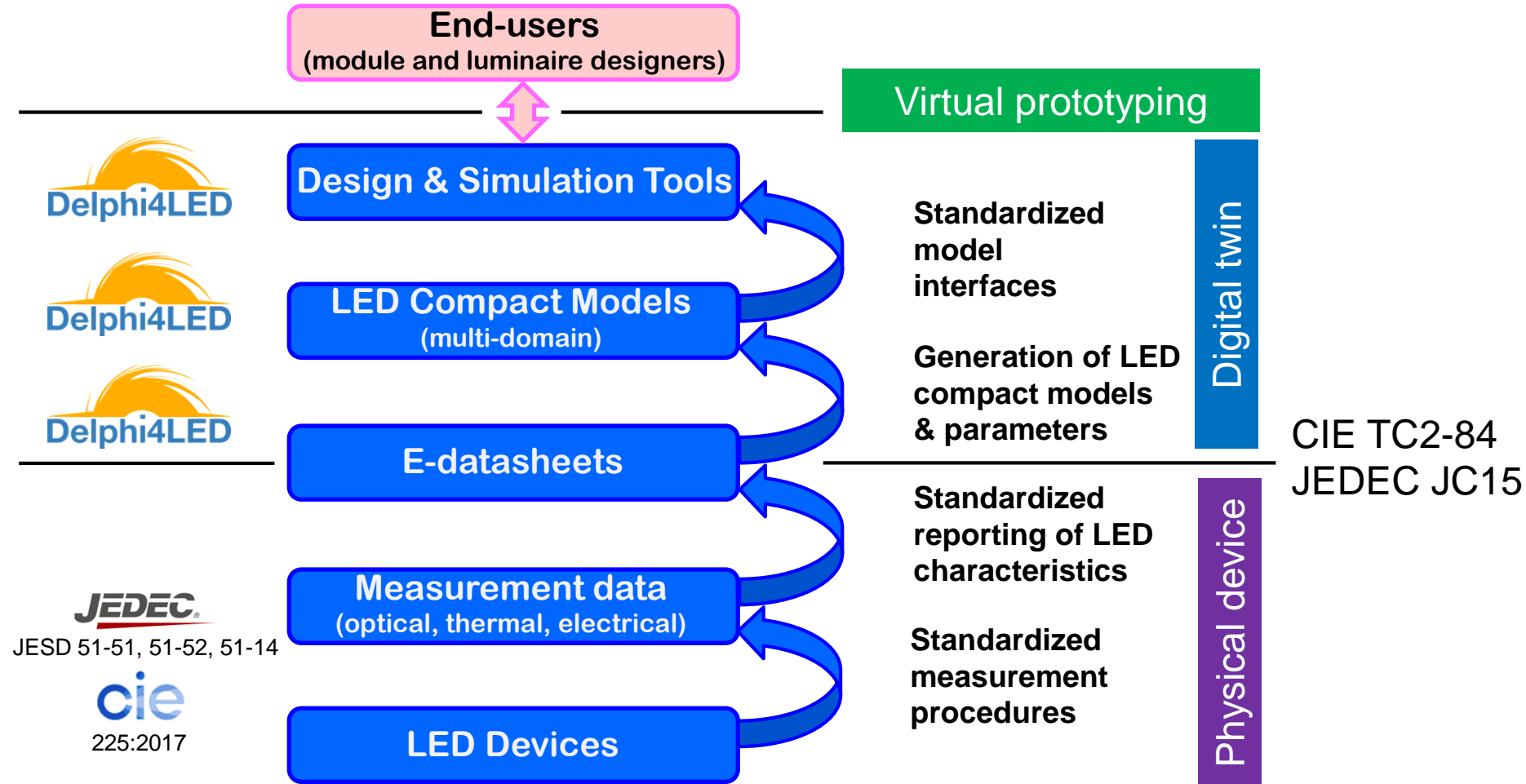
**LED model == digital twin for design**

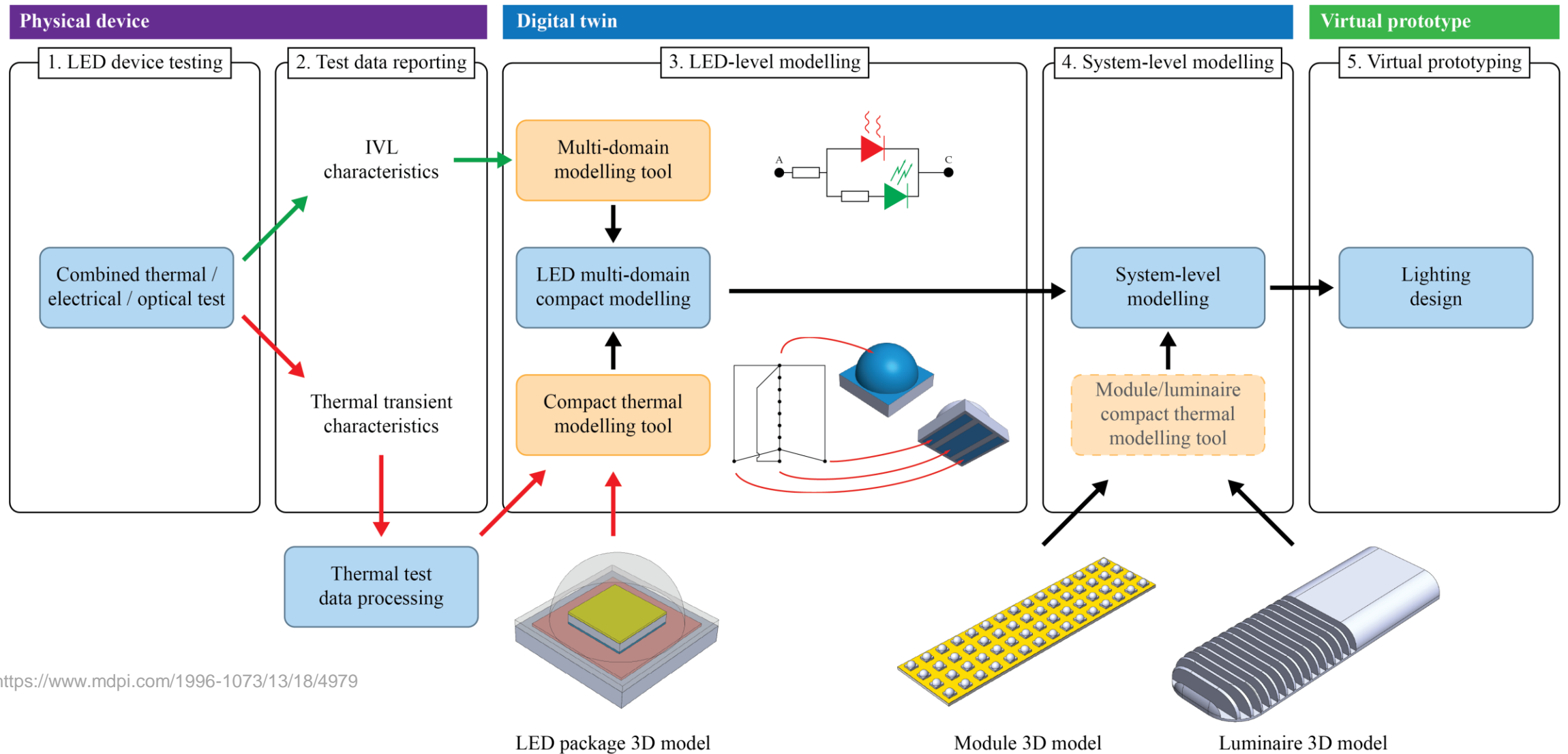
# Using LED digital twins: the first approach in Delphi4LED

The concepts and the major  
research and development results



An Industry 4.0 approach





<https://www.mdpi.com/1996-1073/13/18/4979>

## The major project objectives were

1. Develop **standard methods to create multi-domain LED compact models** from test data
  - Physical samples of LEDs, modules, luminaires replaced by their models
    - **creating digital twins**
2. Improve **simulation of LED thermal, electrical & optical characteristics**
  - **Multi-domain models** at all integration levels using the digital twins
    - bottom-up building of models up to system level (luminaire, lighting system)
3. Reduce design / product cost and time to market
  - Prototype building and physical testing replaced by computer simulation
    - **virtual prototyping**

## Achieved results include new

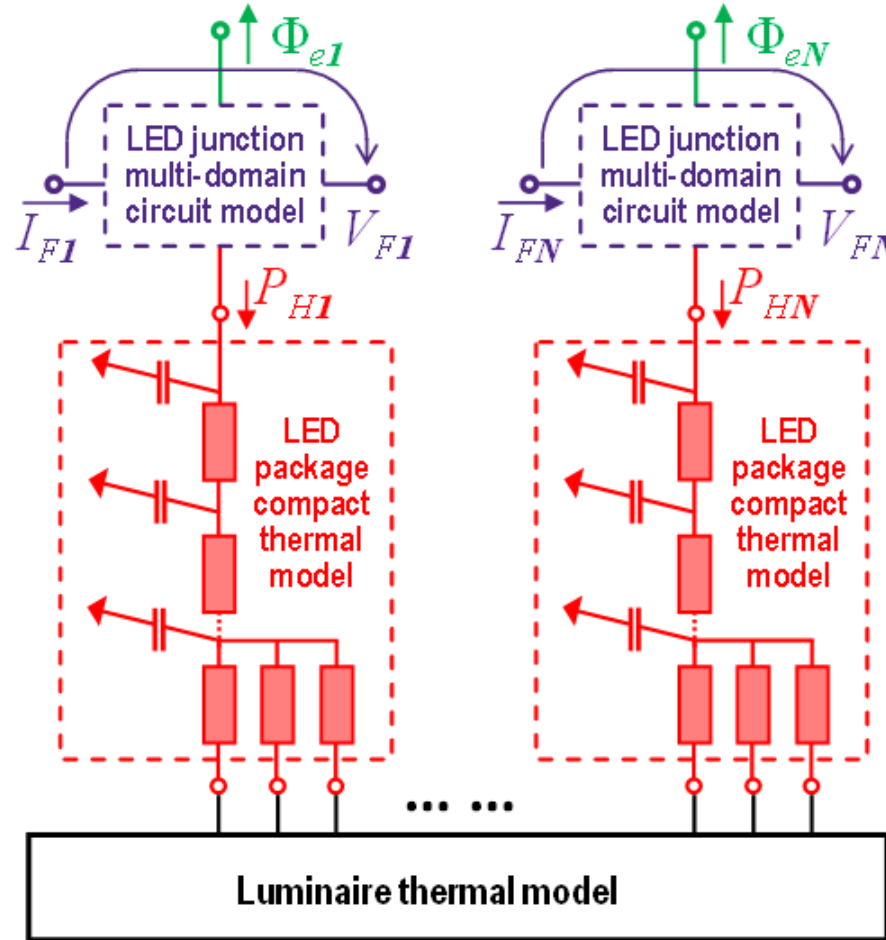
- Testing methods
- Modeling and simulation methods
- **Design workflows**



# The Delphi4LED modular modelling approach

So called boundary condition independent (BCI) models are used on chip and package level.

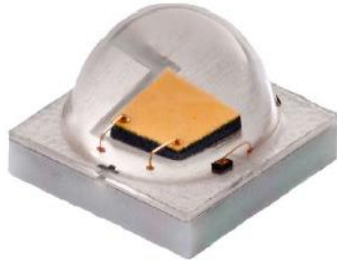
The compact thermal model of the luminaire as a substrate carrying the LED packages usual reflects the wider thermal environment.



Different digital twins on package, module, lamp/luminaire levels

Physical devices

LED package mechanical structure



LED luminaire mechanical structure

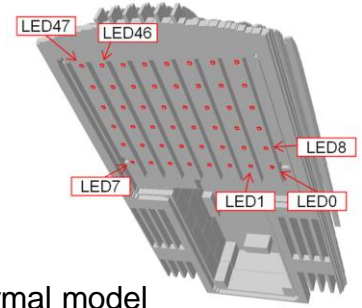
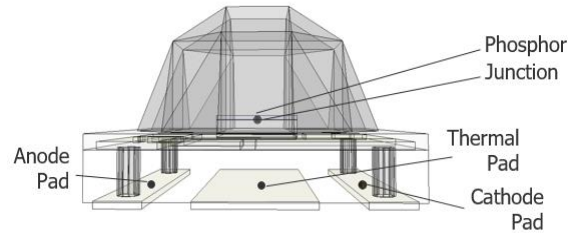
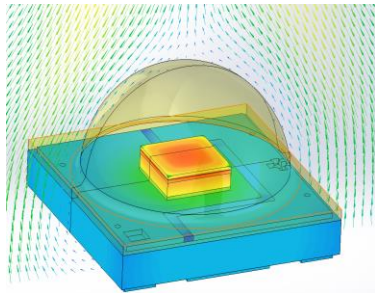


LED luminaire system



Digital twins

Detailed thermal calibrated to thermal transient measurement results

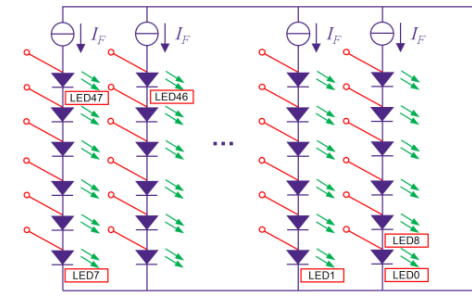
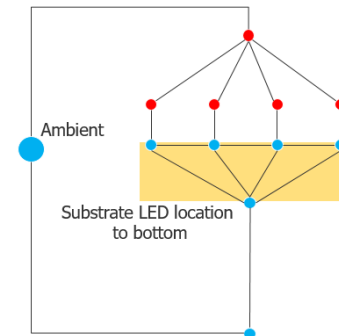
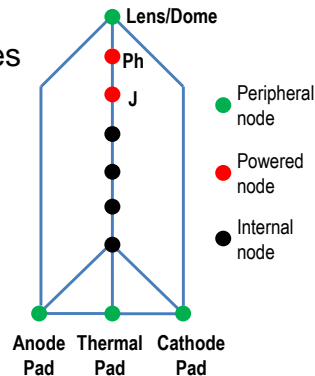
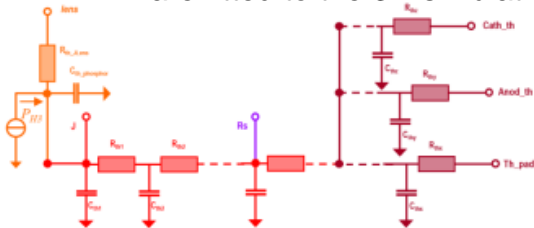


MCAD model → 3D thermal model  
→ compact thermal model

detailed

compact

Compact thermal model element values are fitted to the 3D simulation results



# The Delphi4LED approach: modular modelling

Modular approach / Spice circuit macros corresponding to the integration levels along the SSL supply chain:  
chip – package – substrate/luminaire

## LED chip multi-domain model

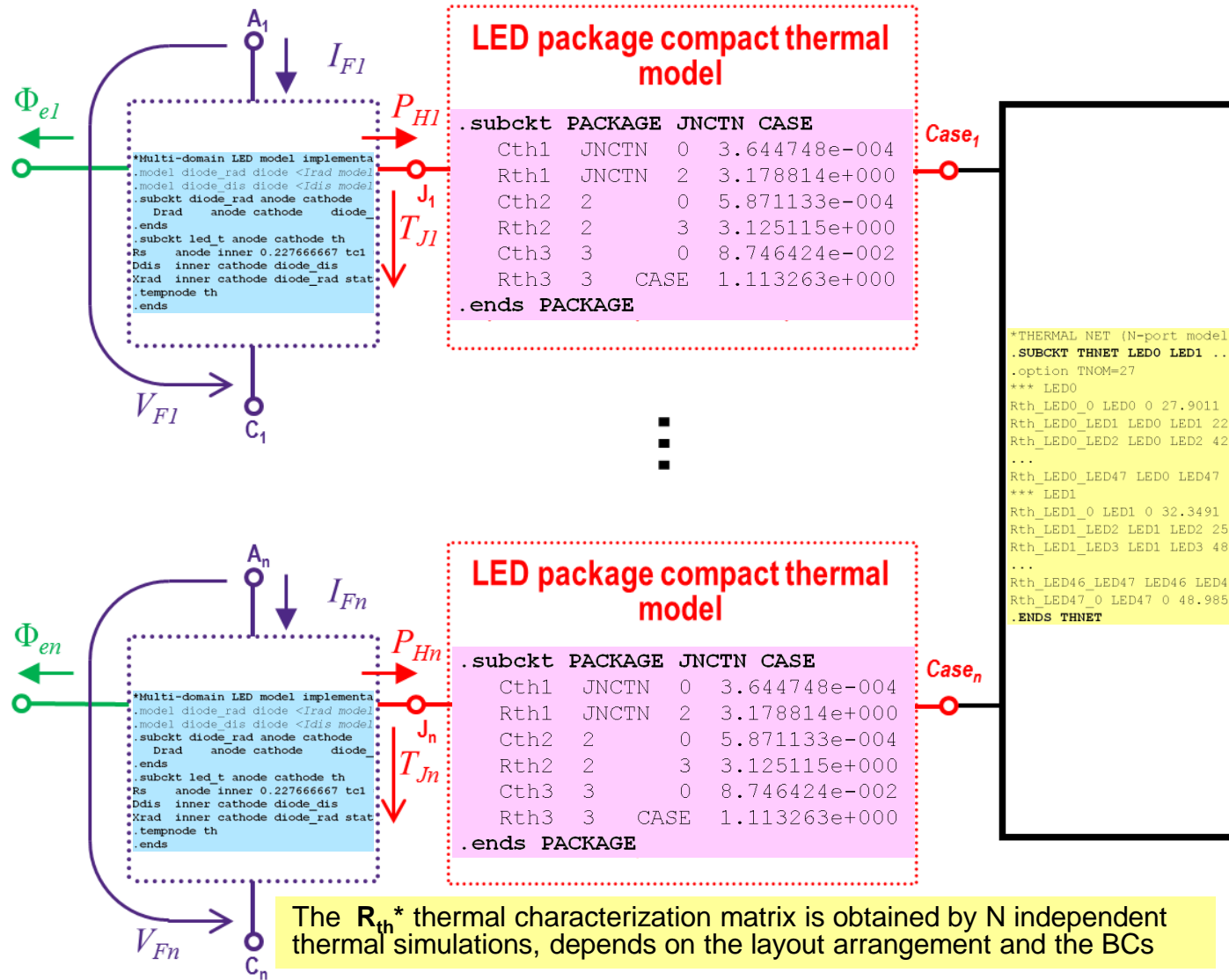
From measured isothermal I-V-L characteristics

## LED package DCTM

Extracted with a “DELPHI” like (JEDEC JESD 15-4) methodology with LED specific model topology and boundary conditions

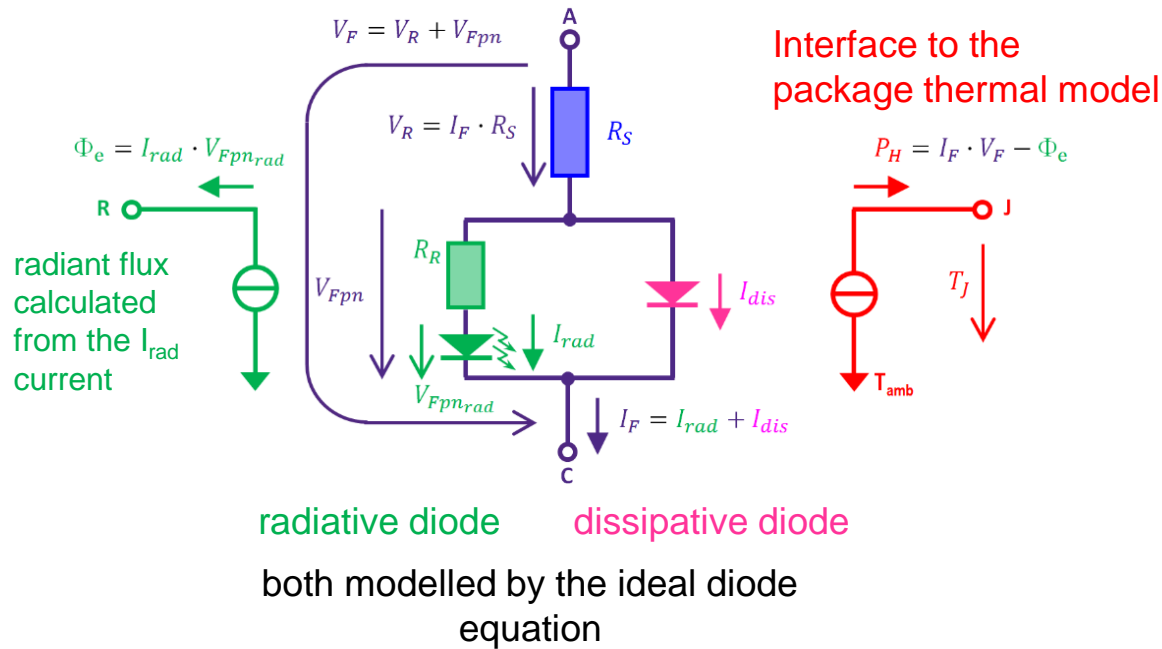
## Substrate / luminaire compact thermal model

Obtained from the  $R_{th}^*$  thermal characterization matrix of a multi heat-source system

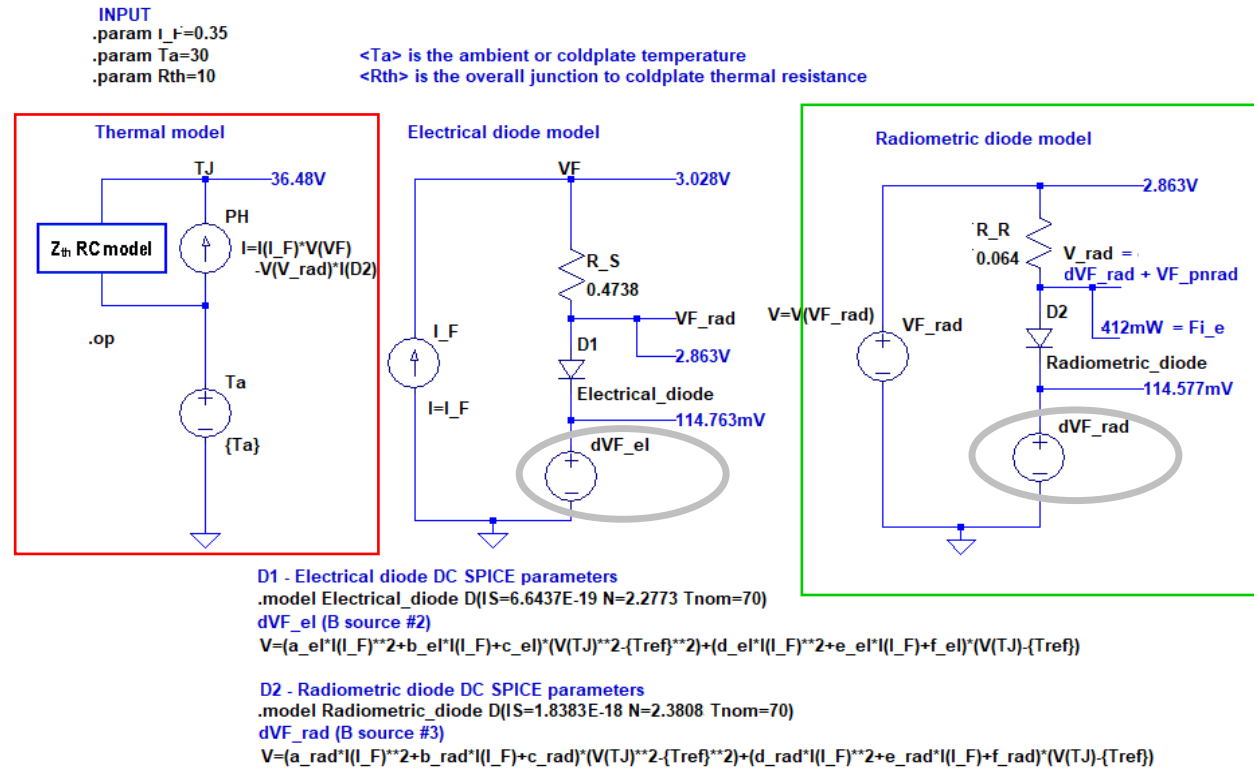


A requirement was to have a model suitable for a generic Spice implementation.

The principle of the model:



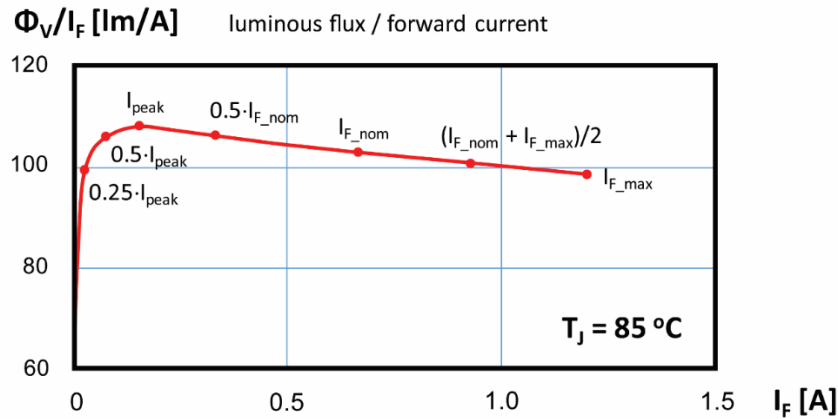
The generic Spice circuit macro implementation:



Implemented as an  $I_F$  forward current driven model, both on level of equations and as a Spice subcircuit macro.

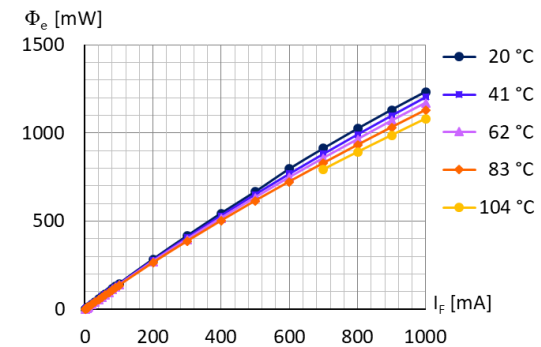
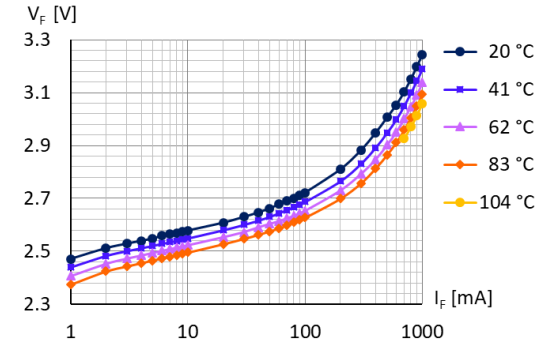
The voltage of the **TJ** node represents the junction temperature. These voltage controlled voltage source represent the  $T_J$  induced change of the diode voltages under constant forward current driving.

The recommended set of the  $(I_F, T_J)$  operating points to which the model has to be fitted during parameter extraction.



34 pairs of  $(I_F, T_J)$

$T_J$ [°C]	30	50	70	85	110
$I_F$ [mA]	20	20	20	20	-
	30	30	30	30	-
	60	60	60	60	-
	100	100	100	100	-
	350	350	350	<b>350</b>	350
	500	500	500	500	500
	-	700	700	700	700
	-	-	1000	1000	1000

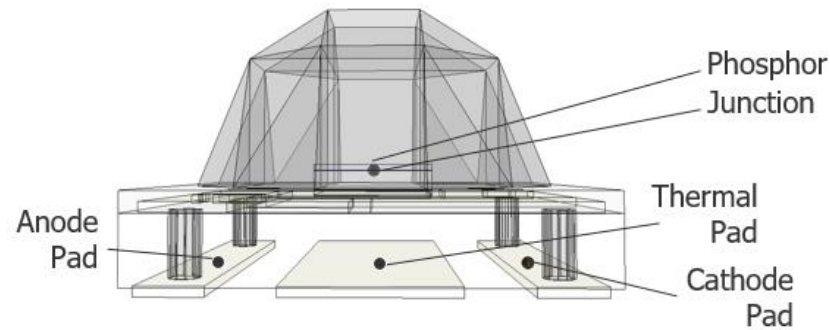


Forward currents to be chosen from both sides of the efficiency/efficacy peak to represent both the low current and high current operating regimes.

The model is expected to provide voltage and flux values with less than 2% relative error in 3 decades of forward current (from the 1 mA range up to the 1000 mA range).

A requirement was to have a model suitable for a generic Spice implementation and suitable also as a compact model for CFD simulation tools.

A 3D model of an LED package with sufficient level of details to properly identify the element values of the dynamic compact thermal model of the package:

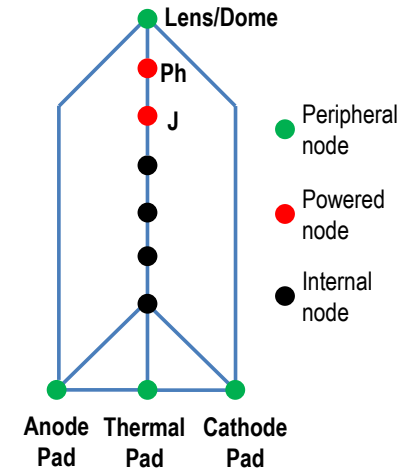


Delphi4LED-style compact thermal model of LED packages.

$$f_{\text{cost}} = \sum_h \sum_i \sum_j \frac{\left( Z_{\text{th,ih}}^{\text{detailed}}(t_j) - Z_{\text{th,ih}}^{\text{CTM}}(t_j) \right)^2}{Z_{\text{th,ih}}^{\text{detailed}}(t_j)}$$

JEDEC DELPHI-style optimization

See JEDEC JESD 15-4



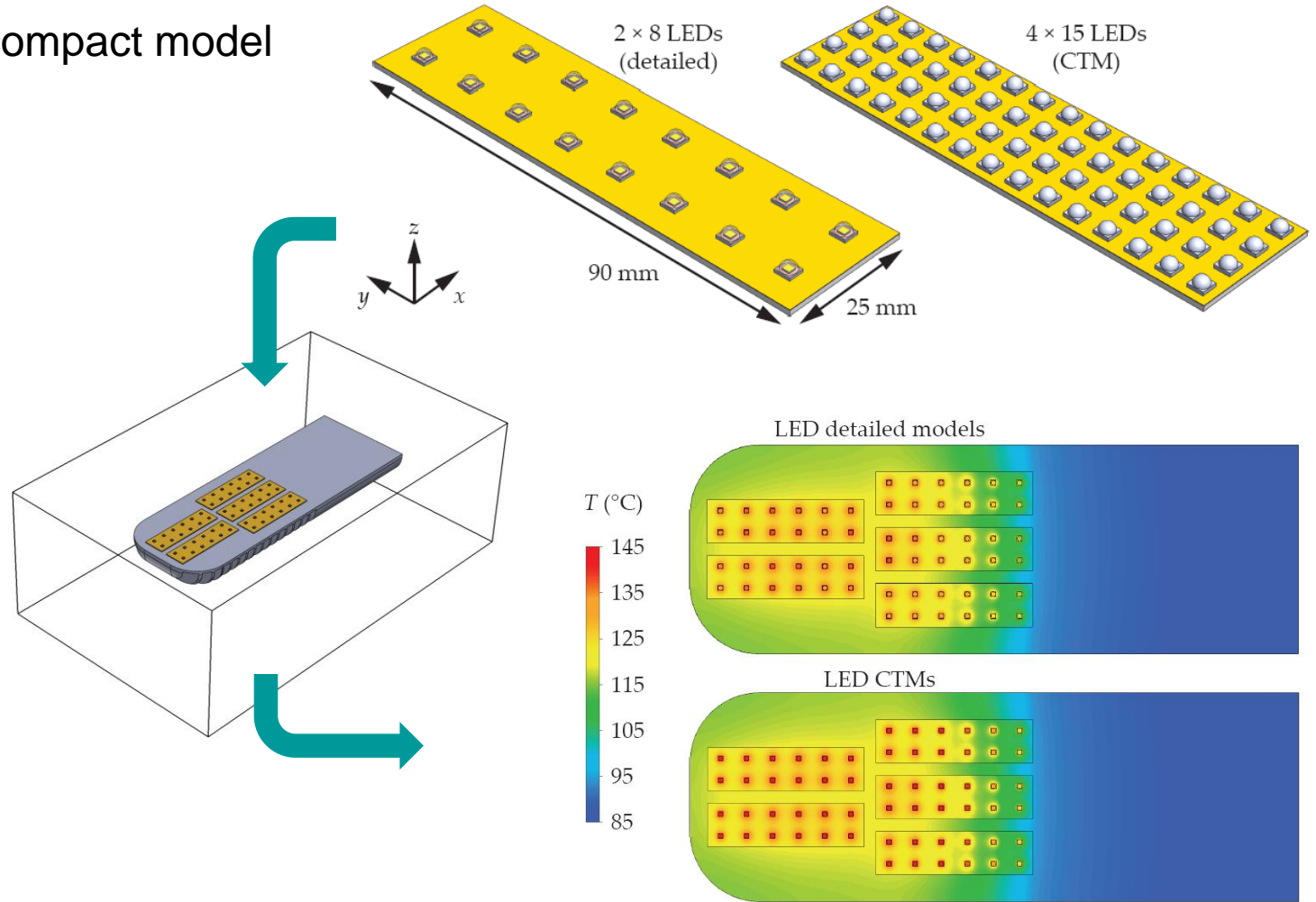
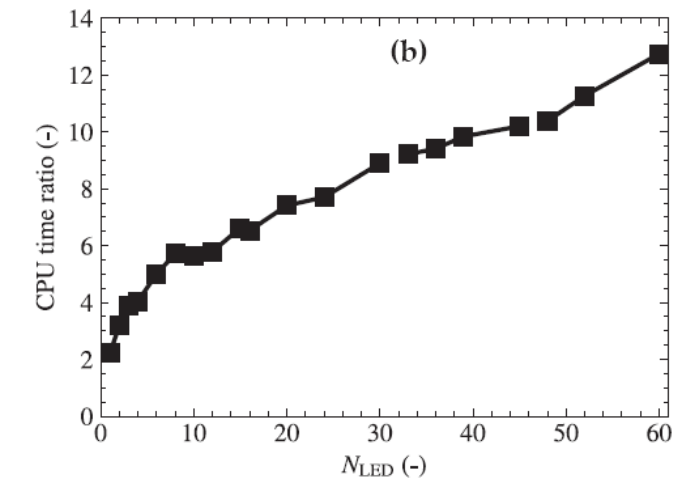
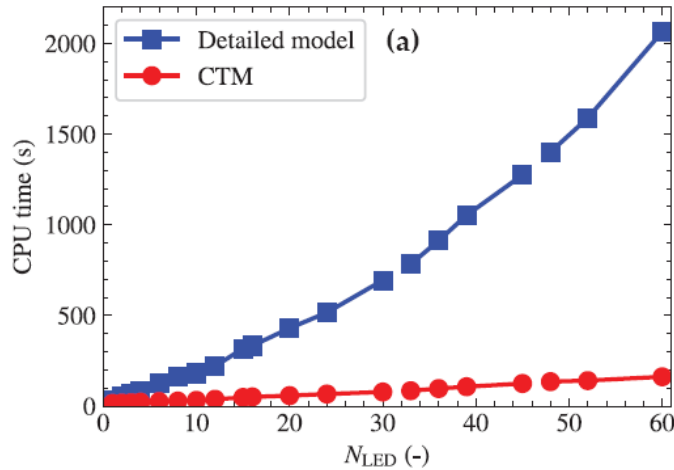
The **model is calibrated** against the **thermal transient test results** of the physical package samples using **structure functions**.

The phosphor can be considered as an additional heat source and the thermal mass of the dome can also be represented in the model.

# Benefits of using compact models (a case-study from Signify, OA, DOI: 10.3390/en13184979)

There are multiple benefits of using compact models instead of detailed ones:

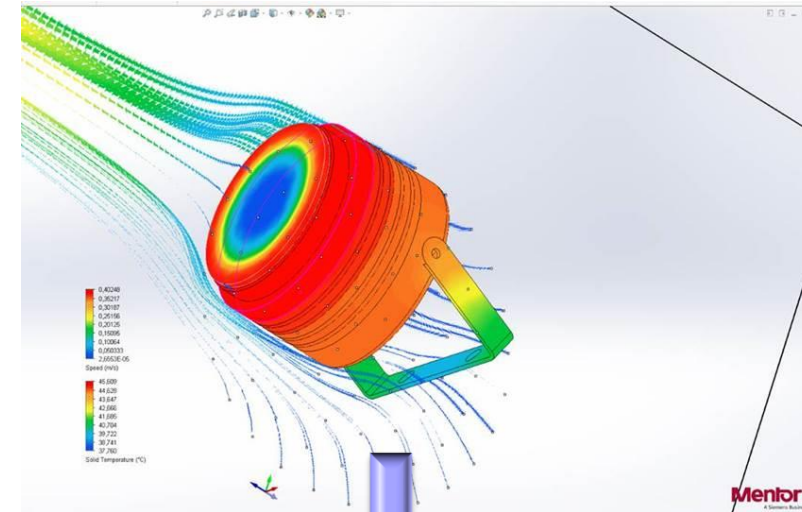
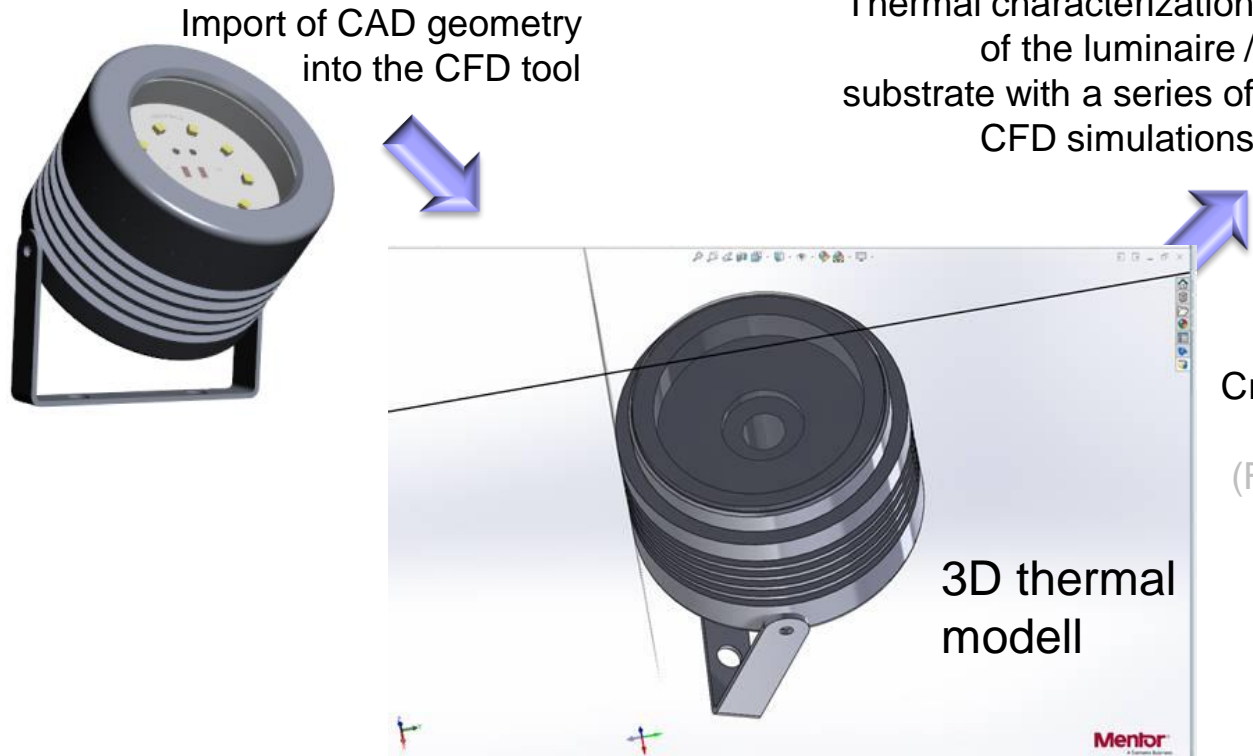
- Reduced computational times
- No proprietary information is found in a compact model



# The Delphi4LED luminaire compact thermal model

A requirement was to have a model suitable for a generic Spice implementation. Such a model can be generated with the  $R_{th}^*$  thermal characterization matrix method or by means of ROM techniques such as published by L. Codecasa as the "FANTASTIC" method.

## MCAD model



Create the  $R_{th}^*$  thermal characterization matrix of luminaire / substrate and conversion to compact model  
(For  $N$  heat-sources an  $N \times N$  matrix by  $N$  CFD simulations)

luminaire / substrate  
thermal compact model in  
Spice netlist format

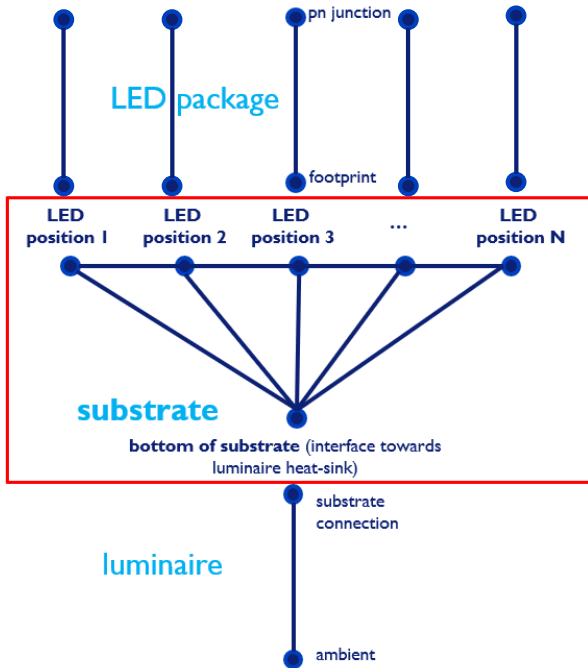
**LED package footprint areas are connected to the footprint nodes of the package compact thermal models**



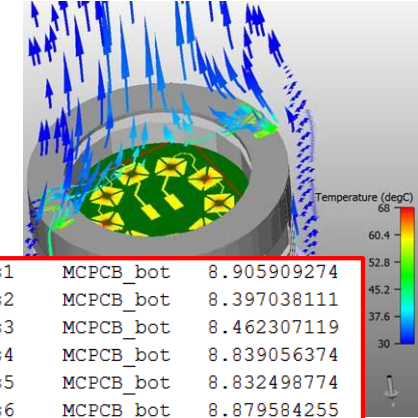
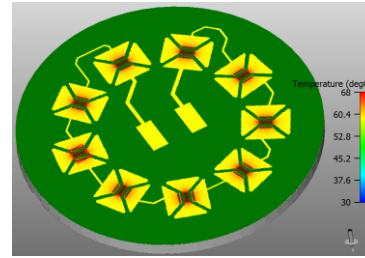
Simplified approach in a so called LED luminaire calculator tools (demo tool as an Excel spreadsheet app)

A demonstrator

- The modelled substrate



Populate the substrate with multi-domain LED package models and study the design alternative on high level with Spice simulations



Rth Matrix Symmetricised						
8.674556331	0.085851129	0.020079796	0.003120538	0.0001	0.0001	0.005169335
0.085851129	8.158273354	0.082818568	0.033955277	0.00688263	0.000846208	0.00063092
0.020079796	0.082818568	8.254507996	0.080956448	0.021946782	0.00155395	0.0001
0.003120538	0.033955277	0.080956448	8.58891142	0.088246138	0.030947062	0.007448014
0.0001	0.00688263	0.021946782	0.088246138	8.591994956	0.089068462	0.032253405
0.0001	0.000846208	0.00155395	0.030947062	0.089068462	8.632464978	0.091306825
0.005169335	0.00063092	0.0001	0.007448014	0.032253405	0.091306825	8.609615549
0.021366075	0.001397169	0.0001	0.0001	0.000969649	0.02402132	0.084291787
0.086297521	0.03532229	0.00519363	0.0001	0.000354614	0.007242548	0.035421427

RPos1MCPCB_bot	Pos1	MCPCB_bot	8.905909274
RPos2MCPCB_bot	Pos2	MCPCB_bot	8.397038111
RPos3MCPCB_bot	Pos3	MCPCB_bot	8.462307119
RPos4MCPCB_bot	Pos4	MCPCB_bot	8.839056374
RPos5MCPCB_bot	Pos5	MCPCB_bot	8.832498774
RPos6MCPCB_bot	Pos6	MCPCB_bot	8.879584255
RPos7MCPCB_bot	Pos7	MCPCB_bot	8.870603828
RPos8MCPCB_bot	Pos8	MCPCB_bot	8.506230548
RPos9MCPCB_bot	Pos9	MCPCB_bot	8.707730701
RPos1Pos2	Pos1	Pos2	829.5982526
RPos2Pos3	Pos2	Pos3	818.3373091
RPos3Pos4	Pos3	Pos4	881.7643185
RPos4Pos5	Pos4	Pos5	841.5554918
RPos5Pos6	Pos5	Pos6	838.6877354
RPos6Pos7	Pos6	Pos7	819.3514046
RPos7Pos8	Pos7	Pos8	853.5095604
RPos8Pos9	Pos8	Pos9	847.774583
RPos9Pos1	Pos9	Pos1	855.5876525
RPos1Pos3	Pos1	Pos3	3740.052540
RPos2Pos4	Pos2	Pos4	2119.052540
RPos3Pos5	Pos3	Pos5	3370.052540
RPos4Pos6	Pos4	Pos6	2475.052540
RPos5Pos7	Pos5	Pos7	2367.052540
RPos6Pos8	Pos6	Pos8	3105.052540
RPos7Pos9	Pos7	Pos9	2111.052540
RPos8Pos1	Pos8	Pos1	3517.052540
RPos9Pos2	Pos9	Pos2	2003.052540

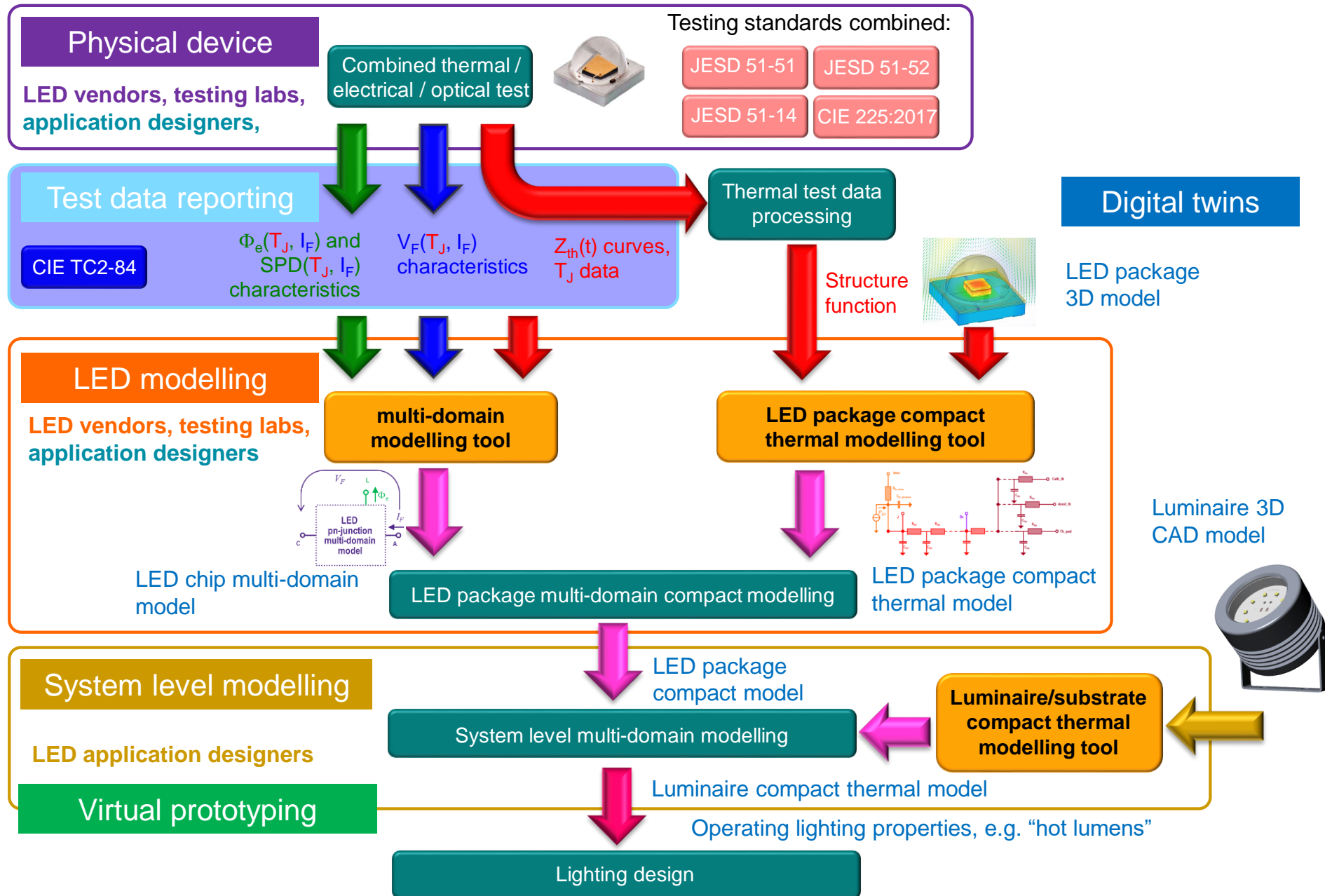
Rth Matrix Inversion						
0.115304596	-0.0012054	-0.00026732	-3.4552E-05	9.58433E-07	1.36726E-06	-6.1535E-05
-0.0012054	0.12260425	-0.00122199	-0.00047178	-9.01E-05	-8.6547E-06	-5.2344E-06
-0.00026732	-0.00122199	0.121170791	-0.00113409	-0.00029673	-1.4541E-05	1.36173E-06
-3.4552E-05	-0.00047178	-0.00113409	0.116455501	-0.00118828	-0.00040401	-9.1959E-05
9.58433E-07	-9.01E-05	-0.00029673	-0.00118828	0.116414387	-0.00119234	-0.00042237
1.36726E-06	-8.6547E-06	-1.4541E-05	-0.00040401	-0.00119234	0.115869403	-0.00122048
-6.1535E-05	-5.2344E-06	1.36173E-06	-9.1959E-05	-0.00042237	-0.00122048	0.116177266
-0.00028433	-1.2421E-05	1.78745E-07	9.96921E-07	-5.8159E-06	-0.00032197	-0.00117163
-0.00116879	-0.00049906	-6.6576E-05	2.41457E-06	-1.4717E-06	-9.0896E-05	-0.00047353

Rth Network Formulation						
8.905909274	829.5982526	3740.853548	28941.82279	-1043369.51	-731392.172	16250.91857
	8.397038111	818.3373091	2119.639289	11098.77527	115543.9267	191045.41
		8.462307119	881.7643185	3370.046818	68769.28145	-734359.432
			8.839056374	841.5554918	2475.190628	10874.46967
				8.832498774	838.6877354	2367.609253
					8.879584255	819.3514046
						8.870603828
						8.506230548
						8.707730701

**LED package footprint areas are connected to the footprint nodes of the package compact thermal models**

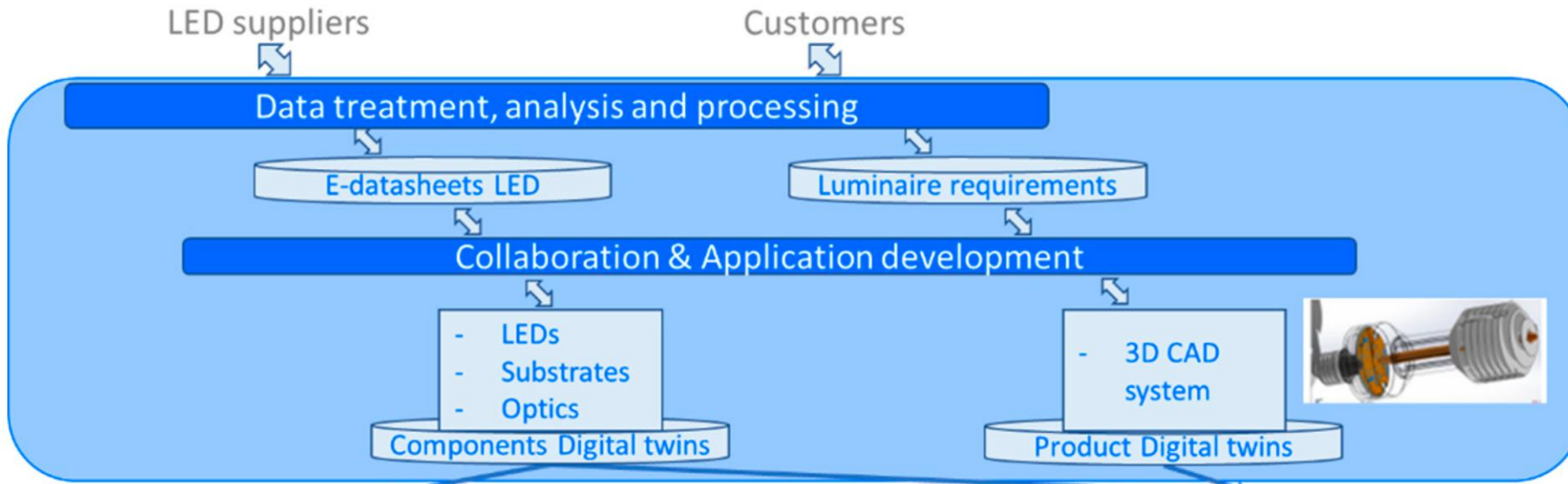
By courtesy of Robin Bornoff (Siemens Digital Industry Software Simulation and Test Solutions Strategy and Innovation, Technology Innovation group)

# Digital twins on multiple integration levels – in a digitalized development workflow



# First implementations – two foreseen options for different company environments

With the vision of component libraries available from vendors (LEDs, drivers, etc.)

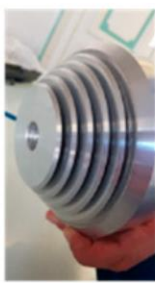


### SME Luminaire calculator (e.g. excel)

GOALS	
Luminous Flux (lm)	1200
CONSTRAINTS	
Tj max (degC)	150
Ts max (degC)	85
Ta (degC)	45
Max Overall Forward Voltage (V)	50
DESIGN	
Number of LEDs	6
Substrate Type	SMD
HeatSink Rth (K/W)	2.3
Forward Current (A)	1.1
Optics Efficiency	0.8

**SIMULATE**

RESULTS	
Highest Tj (degC)	92.6
Highest Ts (degC)	84.2
Total Luminous Flux (lm)	1392
Total Optical Power (mW)	5305
Max Overall Forward Voltage (V)	20.3



### Major Product system modelling Spice-like simulations + 3D simulations

```

RPos1MCPCB_bot Pos1 MCPCB_bot 8.905909274
RPos2MCPCB_bot Pos2 MCPCB_bot 8.397038111
RPos3MCPCB_bot Pos3 MCPCB_bot 8.442307119
RPos4MCPCB_bot Pos4 MCPCB_bot 8.03905437
RPos5MCPCB_bot Pos5 MCPCB_bot 8.0324907
RPos6MCPCB_bot Pos6 MCPCB_bot 8.079584255
RPos7MCPCB_bot Pos7 MCPCB_bot 8.070403828
RPos8MCPCB_bot Pos8 MCPCB_bot 8.504230548
RPos9MCPCB_bot Pos9 MCPCB_bot 8.707730701
RPos1Pos2 Pos1 Pos2 829.5982526
RPos2Pos3 Pos2 Pos3 819.3373091
RPos3Pos4 Pos3 Pos4 881.7443285
RPos4Pos5 Pos4 Pos5 841.5554918
RPos5Pos6 Pos5 Pos6 838.4877354
    
```

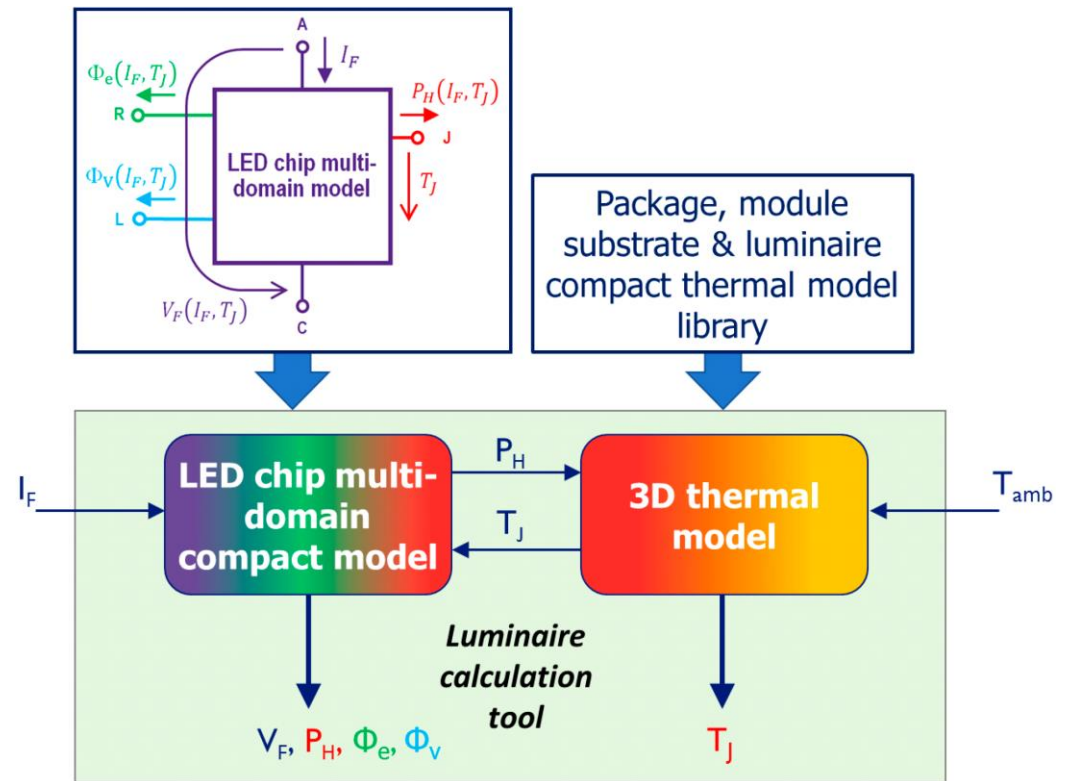
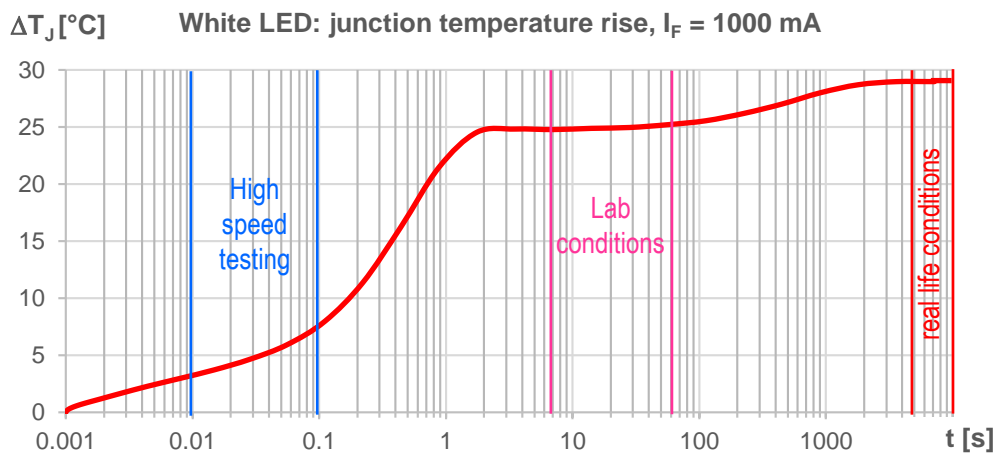
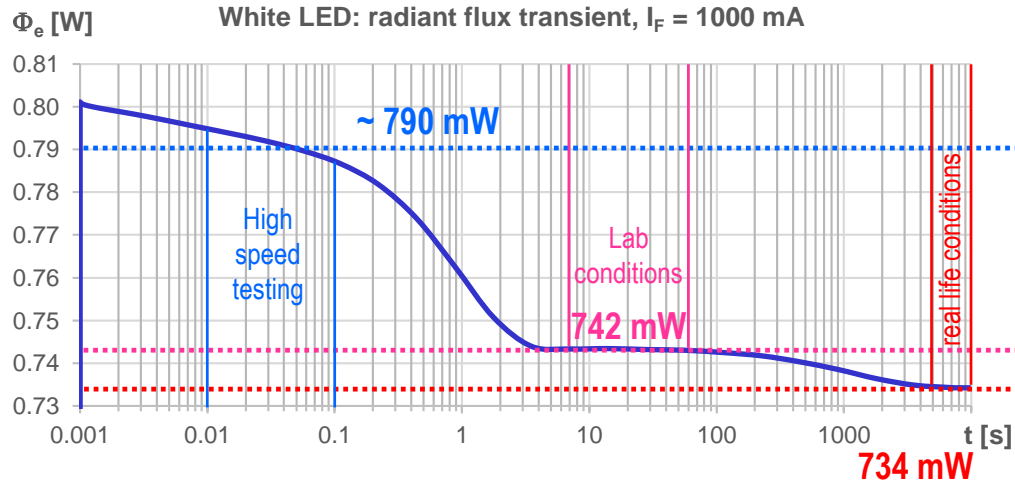


<https://www.mdpi.com/1996-1073/12/12/2389/htm>

# First implementations – trials with two options for different company environments

All models merged in a Spice netlist and simulated with Spice only (direct method) → *any signal for any driving mode...*

Electrical and thermal solvers iterate (relaxation method). Demo tool in an Excel spreadsheet application → *quick evaluation of basic design choices*



<https://www.mdpi.com/1996-1073/12/12/2389/htm>

# First implementations – luminaire design calculator

1. Set design goals/objectives (total flux)
2. Define (temperature) constraints
3. Enter design choices
4. Simulate and evaluate

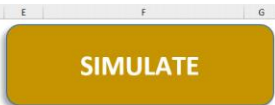
GOALS	
Luminous Flux (lm)	1200
CONSTRAINTS	
Tj max (degC)	150
Ts max (degC)	85
Ta (degC)	45
Max Overall Forward Voltage (V)	50
DESIGN	
Number of LEDs	5
Substrate Type	SMI 5W
Heatsink Rth (K/W)	2,3
Forward Current (A)	1,1
Optics Efficiency	0,8



RESULTS	
Highest Tj (degC)	89,9
Highest Ts (degC)	81,5
Total Luminous Flux (lm)	1170
Total Optical Power (mW)	4433
Max Overall Forward Voltage (V)	16,8

*Total luminous flux target not met*

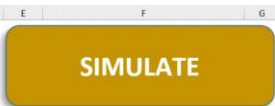
GOALS	
Luminous Flux (lm)	1200
CONSTRAINTS	
Tj max (degC)	150
Ts max (degC)	85
Ta (degC)	45
Max Overall Forward Voltage (V)	50
DESIGN	
Number of LEDs	6
Substrate Type	SMI 5W
Heatsink Rth (K/W)	2,3
Forward Current (A)	1,1
Optics Efficiency	0,8



RESULTS	
Highest Tj (degC)	95,3
Highest Ts (degC)	86,9
Total Luminous Flux (lm)	1395
Total Optical Power (mW)	5291
Max Overall Forward Voltage (V)	20,1

*Solder point temperature constraint violated*

GOALS	
Luminous Flux (lm)	1200
CONSTRAINTS	
Tj max (degC)	150
Ts max (degC)	85
Ta (degC)	45
Max Overall Forward Voltage (V)	50
DESIGN	
Number of LEDs	6
Substrate Type	SMI 8W
Heatsink Rth (K/W)	2,3
Forward Current (A)	1,1
Optics Efficiency	0,8



RESULTS	
Highest Tj (degC)	92,6
Highest Ts (degC)	84,2
Total Luminous Flux (lm)	1399
Total Optical Power (mW)	5305
Max Overall Forward Voltage (V)	20,1

*Design target met without violation of constraints*

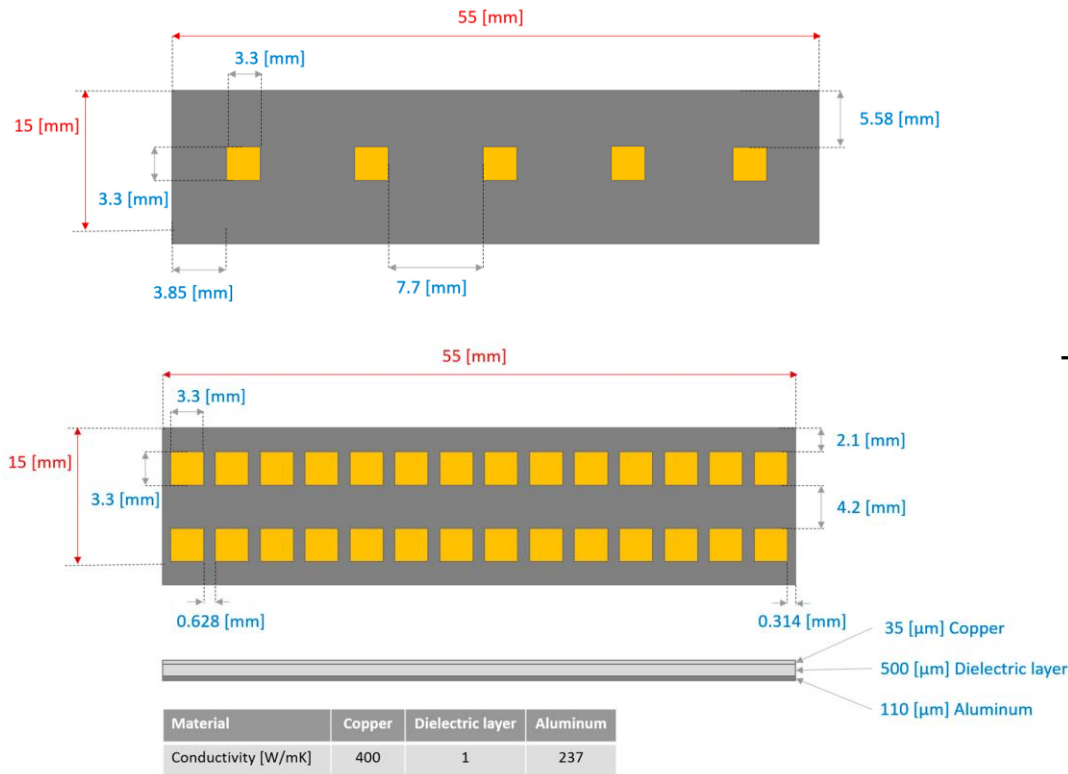
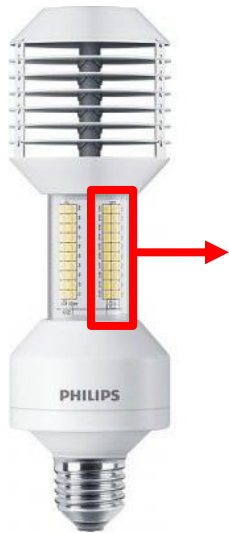
GOALS	
Luminous Flux (lm)	1200
CONSTRAINTS	
Tj max (degC)	150
Ts max (degC)	85
Ta (degC)	45
Total Power Consumption (W)	15
DESIGN	
Number of LEDs	6
Substrate Type	SMI 3W
Heatsink Rth (K/W)	2.5
Forward Current (A)	1.5
Optics Efficiency	0.8
Driver Efficiency	0.9
RESULTS	
Highest Tj (degC)	85.38
Highest Ts (degC)	79.27
Total System Power Consumption (W)	29.96
Total System Luminous Flux (lm)	2465
Total Luminous Flux from LEDs (lm)	3082
Total System Optical Power (mW)	7582
Total Optical Power from LEDs (mW)	9478
Total System Lumens/Watt (lm/W)	82.28
Total Lumens/Watt from LEDs (lm/W)	113.1

PER LED RESULTS	Vf (V)	Luminous Flux (lm)	Tj (DegC)	Ts (DegC)	P (W)	Pdis (W)
1	3.03	513.47	85.38	79.27	4.5	2.96
2	3.03	513.69	85.17	78.84	4.5	2.96
3	3.03	513.61	85.25	79.00	4.5	2.96
4	3.03	513.63	85.23	78.96	4.5	2.96
5	3.03	513.62	85.24	78.98	4.5	2.96
6	3.03	513.65	85.21	78.92	4.5	2.96

Demo example, following the architecture of the 70 W HPS replacement lamp

Design choices were:

1. Type A or Type B LED?
2. Smaller number of LEDs driven by higher current (less mfg. cost, smaller LED efficiency) or higher number of LEDs driven by a smaller current (more mfg. cost, higher LED efficiency)



## Type A

Calculated Property	5 LEDs; $I_F = 500 \text{ mA}$	22 LEDs; $I_F = 100 \text{ mA}$
Solder point temperature [°C]	51.6	46.9
Junction temperature [°C]	54.3	47.3
Light output per PCB [lm]	1056	1049
Total Light output [lm]	6336	6294
Efficacy [lm/W]	150	180

## Type B

Calculated Property	5 LEDs; $I_F = 200 \text{ mA}$	22 LEDs; $I_F = 60 \text{ mA}$
Solder point temperature [°C]	51.8	47.6
Junction temperature [°C]	61.1	49.7
Light output per PCB [lm]	664	1008
Total Light output [lm]	3984	6050
Efficacy [lm/W]	105	136

# Evaluating the benefits

Benefits of the digitalized development flow: reduced development time and cost.  
 Overall gain is 28% (SME environment) .. 42% (major company environment)

## Demo experiments in Delphi4LED:

Main design costs	"SME" old process	"SME" new proces	Gain
Personal costs	0.896	0.633	29%
Material costs	0.049	0.028	43%
Testing	0.056	0.056	0%
<b>Total</b>	1.000	0.717	<b>28%</b>
Main design costs	"Major" old process	"Major" new proces	Gain
Personal costs	0.819	0.502	39%
Material costs	0.055	0.028	48%
Testing	0.126	0.045	65%
<b>Total</b>	1.000	0.575	<b>42%</b>



**SIMULATE**

RESULTS	
Highest Tj (degC)	47.55
Highest Ts (degC)	43.33
Total System Power Consumption (W)	11.71
Total System Luminous Flux (lm)	1302
Total Luminous Flux from LEDs (lm)	1628
Total System Optical Power (mW)	3971
Total Optical Power from LEDs (mW)	4964
Total System Lumens/Watt (lm/W)	111.2
Total Lumens/Watt from LEDs (lm/W)	139

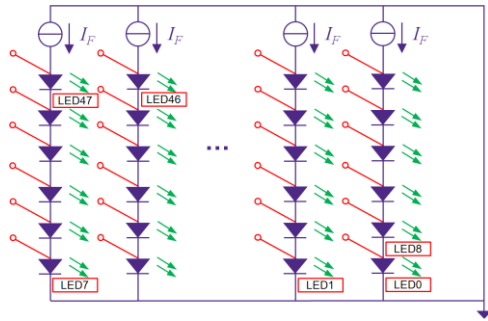
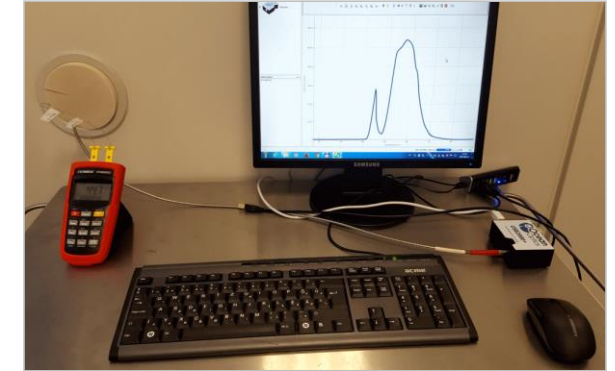
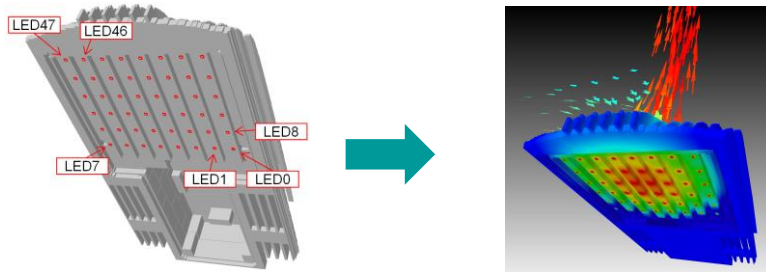
10,7W measured  
1339 lm measured

Simulated major performance indicators were confirmed by measurements

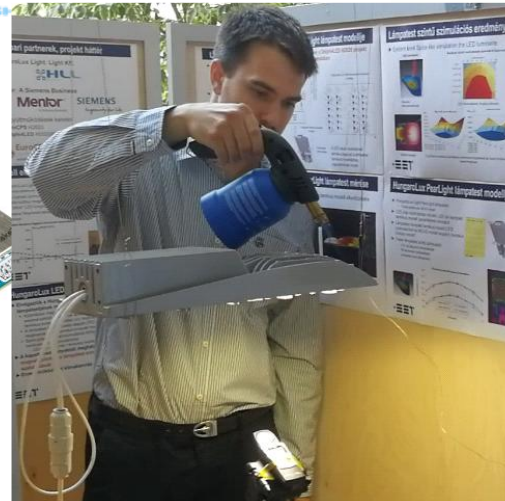
# Yet another application example: a smart luminaire with temperature compensated CLO

**Background:** street-lighting luminaires have to provide required level of illumination of roads, even under the *worst case conditions* → hottest summer night / least efficient LED operation → over-lighting most of the year

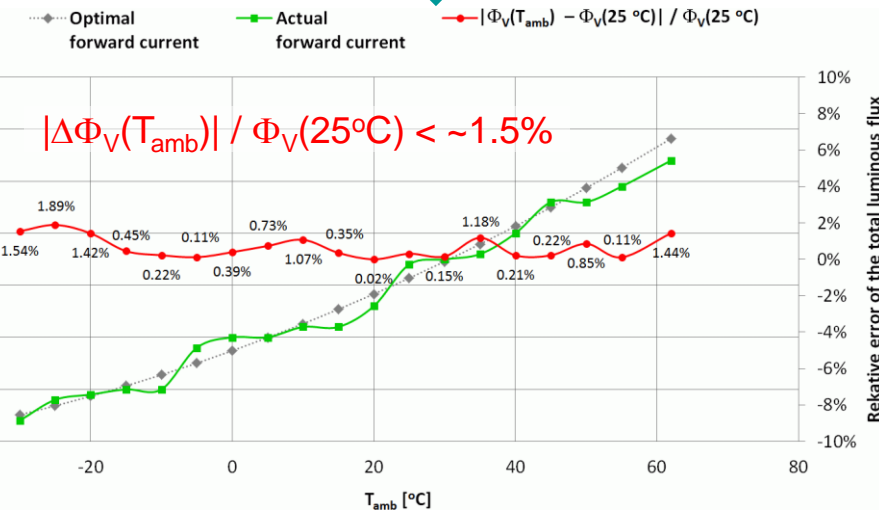
Finding the  $I_F(T_{amb})|_{\Phi=const}$  function:



HUNGAROLUX



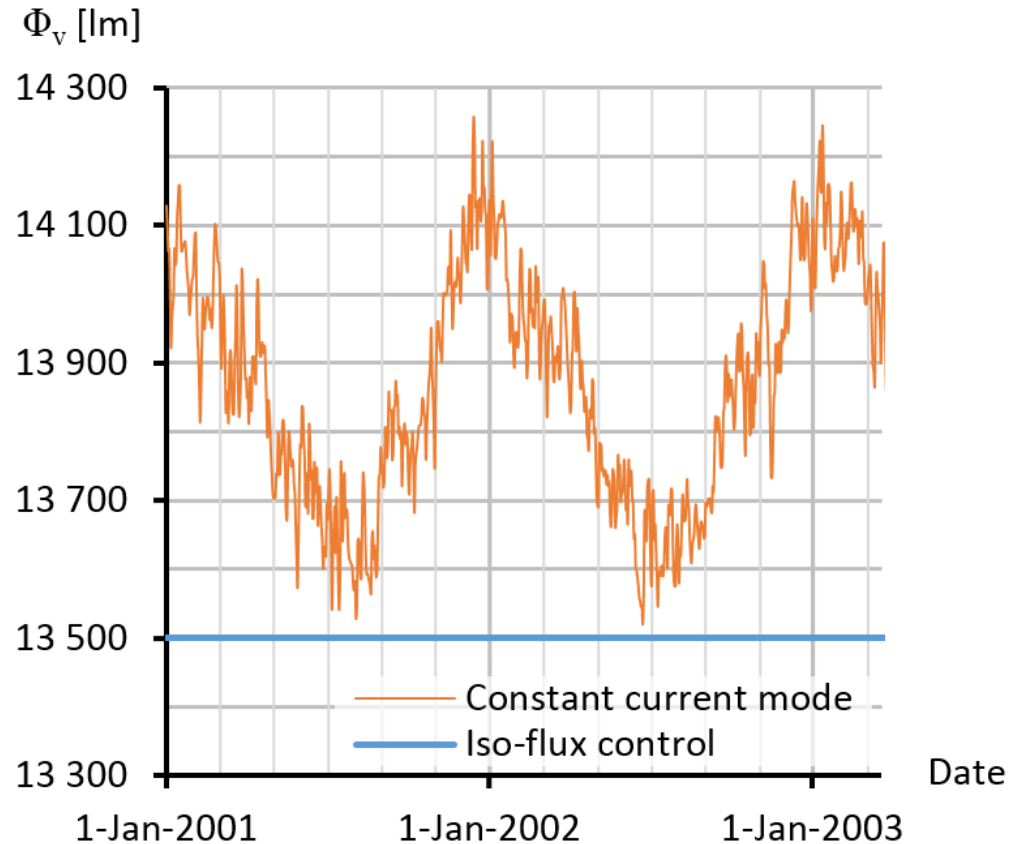
Delphi4LED type modelling and simulation was performed → results converted into an embedded model





# Annual $\Phi_v$ variation with/without CLO control

- ▶ Simulated light output variation during a year: 6-8%
  - $T_A$  taken from archived met data of Szombathely, Hungary



Though in the public domain, **Delphi4LED models did not become widespread**

- The **measurement of a set of isothermal IVL characteristics for 34 operating points** for pre-defined ( $I_F$ ,  $T_J$ ) pairs is not yet a common practice
  - The measurements comply with the most recent JEDEC standards and CIE recommendations and an automated procedure is available in commercial measurement tools.
  - With these, the full characterization of an LED package **is impedingly long**, it takes ~8 hours
- Measurement results are not reported in a standard electronic data format
  - **CIE TC2-84, JEDEC JC15 committee work in progress...**
- There is no efficient parameter extraction tool available
  - **needs for an improved test method, for a standard data format, for a parameter extraction tool...**
- The Delphi4LED type **multi-domain digital twin of LEDs is valid for the 0 of operation**
  - **add at least the elapsed product lifetime as a further model parameter...**
  - **add lifetime / reliability aspects on luminaire level too...**

Modelling the LED drivers was missing

→ **add LED driver models with electro-thermal features and connect them to reliability prediction...**

Only total fluxes were calculated

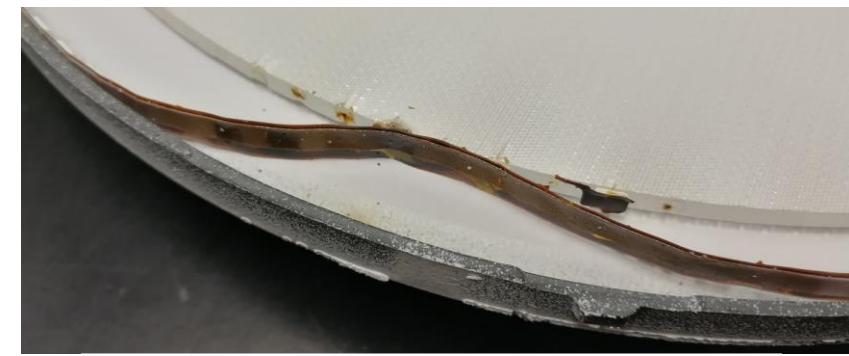
→ **add at current, temperature and lifetime dependent spectrum model...**

Too simplistic luminaire level model, only the effect of the static thermal environment was considered

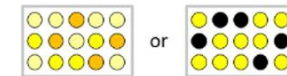
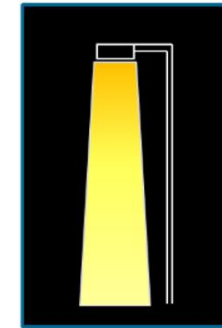
→ **find ways of considering the mission profile of luminaires to predict RUL...**

# Extend the Delphi4LED concepts with lifetime/reliability aspects towards lifetime prediction during operation

The approach of **AI-TWILIGHT**, a new European project

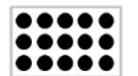
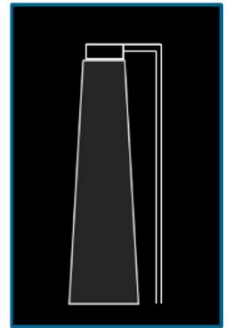


degradation

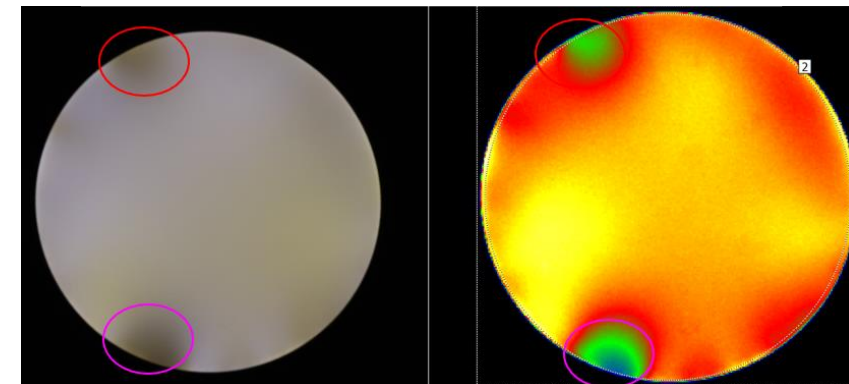


Lumen / colour maintenance of LED-based luminaire

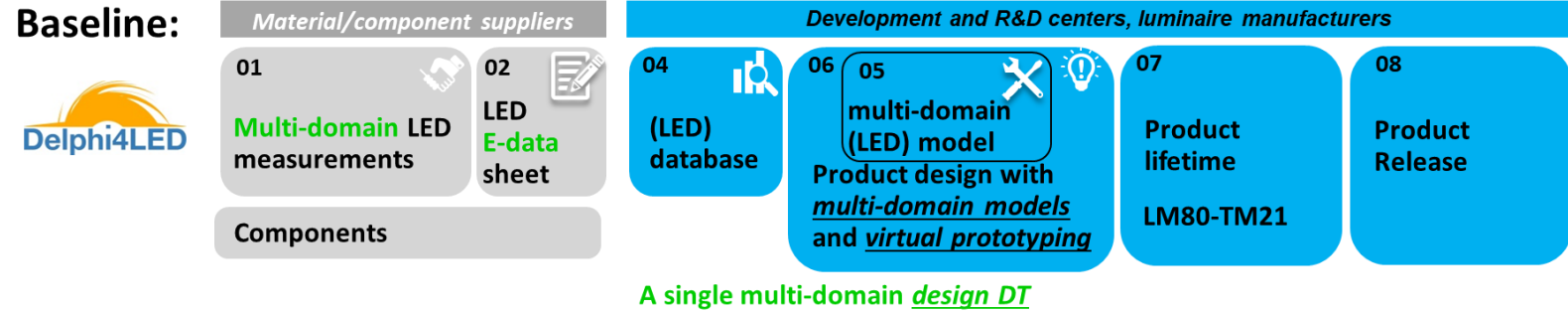
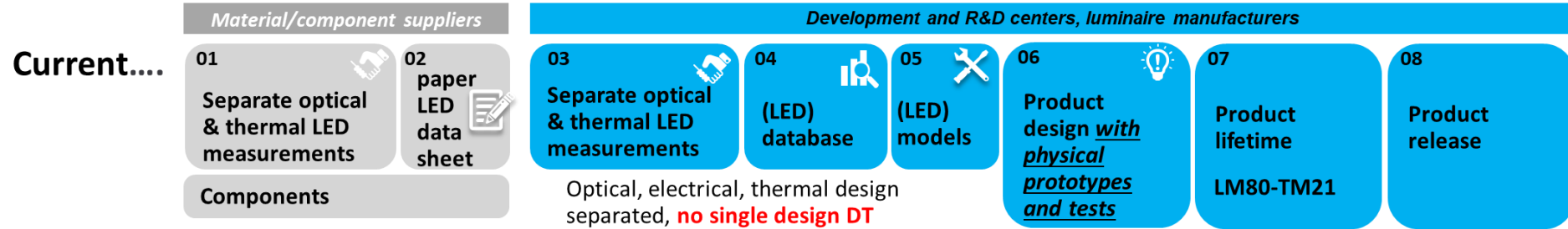
catastrophic



complete failure of LED-based luminaire

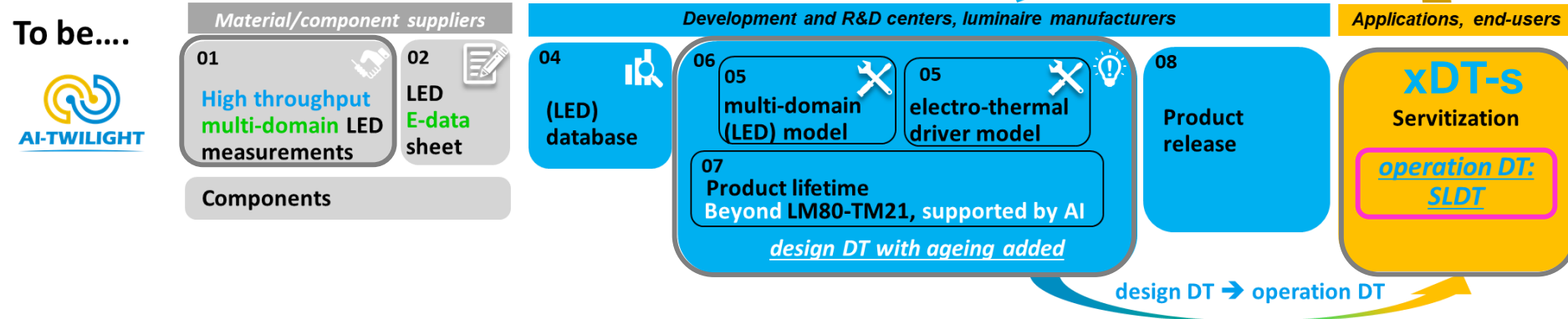


# The baseline and vision of AI-TWILIGHT:



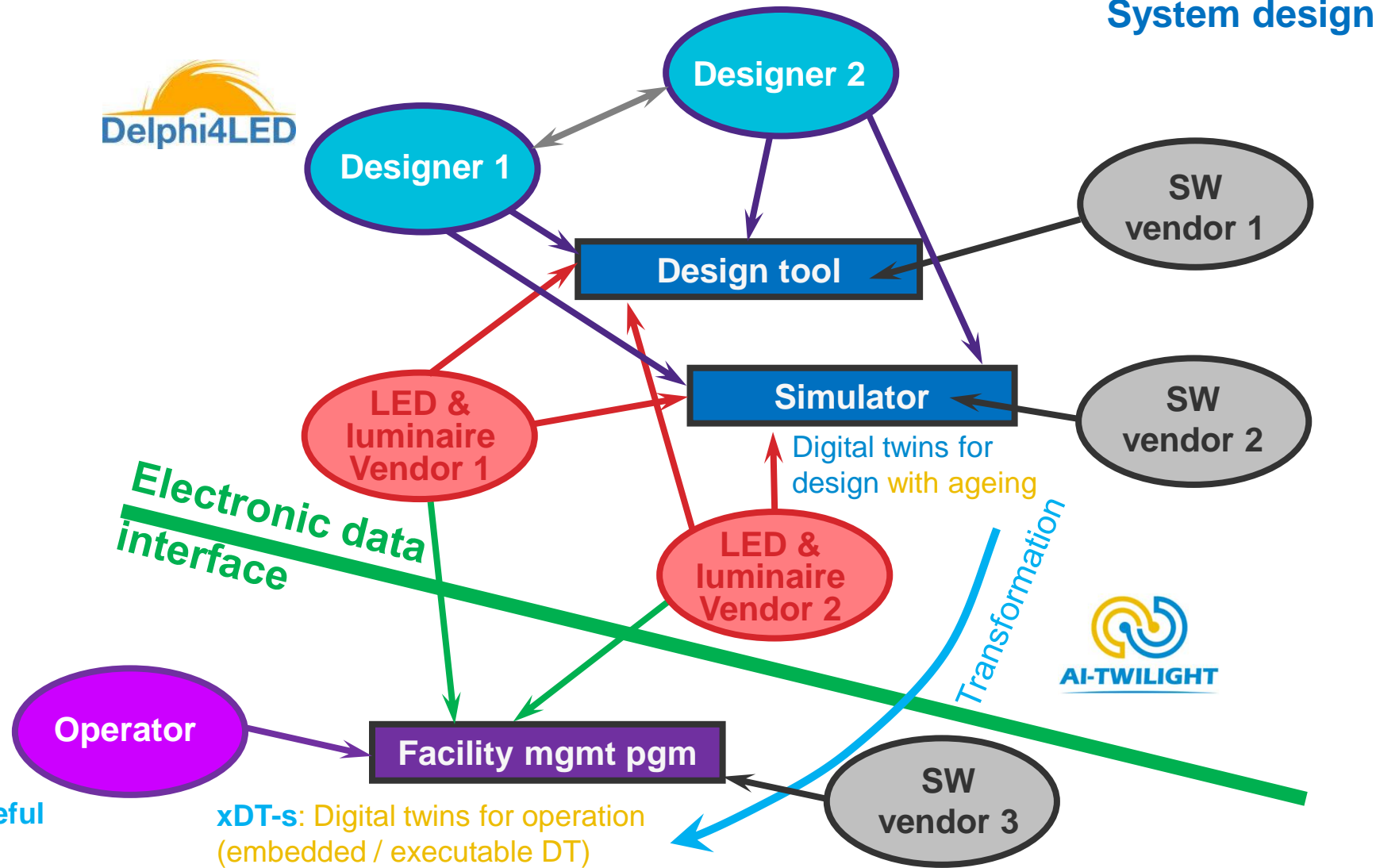
The use of the Delphi4LED workflow has been successfully demonstrated.

Delphi4LED methodologies are not yet widespread... (testing throughput and parameter extraction issues)



Apply AI methods in creating models for *predictive / prescriptive maintenance* and LED product *lifetime prediction*.

# The wider vision: Lighting 4.0 with AI support



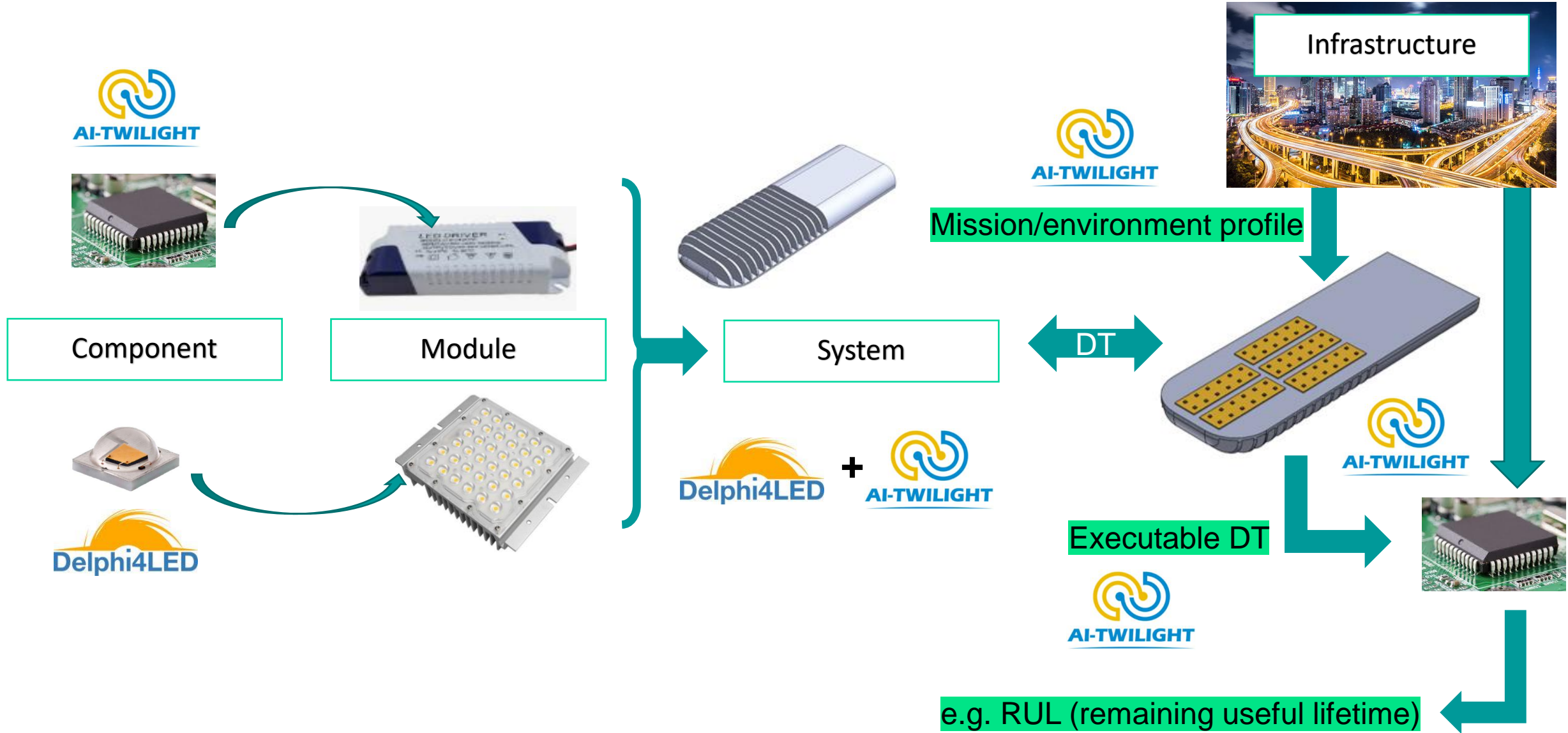
## Lighting system operation



Life-time modelling and prediction of remaining useful life time supported by AI methods



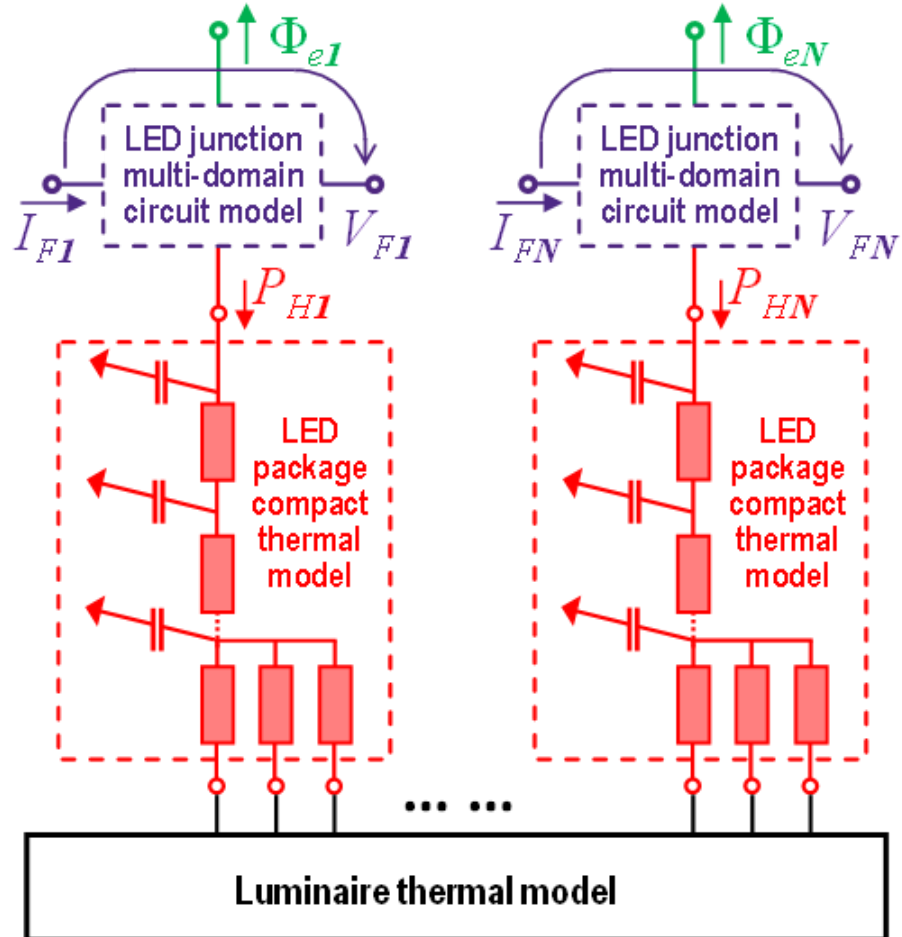
# The extended approach: digital twin (DT) for design and for operation



# Adding new items to the former Delphi4LED modules (digital twins for design)

transformation into an xDT

add SPD model extended with ageing (possible inputs:  $I_F$ ,  $T_J$ ,  $\Phi_e$ , elapsed lifetime)



add driver model to the overall luminaire model

consider ageing in the diode characteristics (e.g. elapsed lifetime as parameter)

model the degradation of the heat-flow path (e.g. elapsed lifetime as parameter)

create different transfer functions for the executable version of the DT, etc.

add ageing to the models

# | Some details of the work done so far...

Focusing on data analysis and modelling issues

Discussing the foreseen improvement of tests requires another talk of about 40 min.



# Some steps taken forward: parameter extraction for the chip level multi-domain model

Global optimization in a 18 dimensional space with a procedure based on the Nelder-Mead method

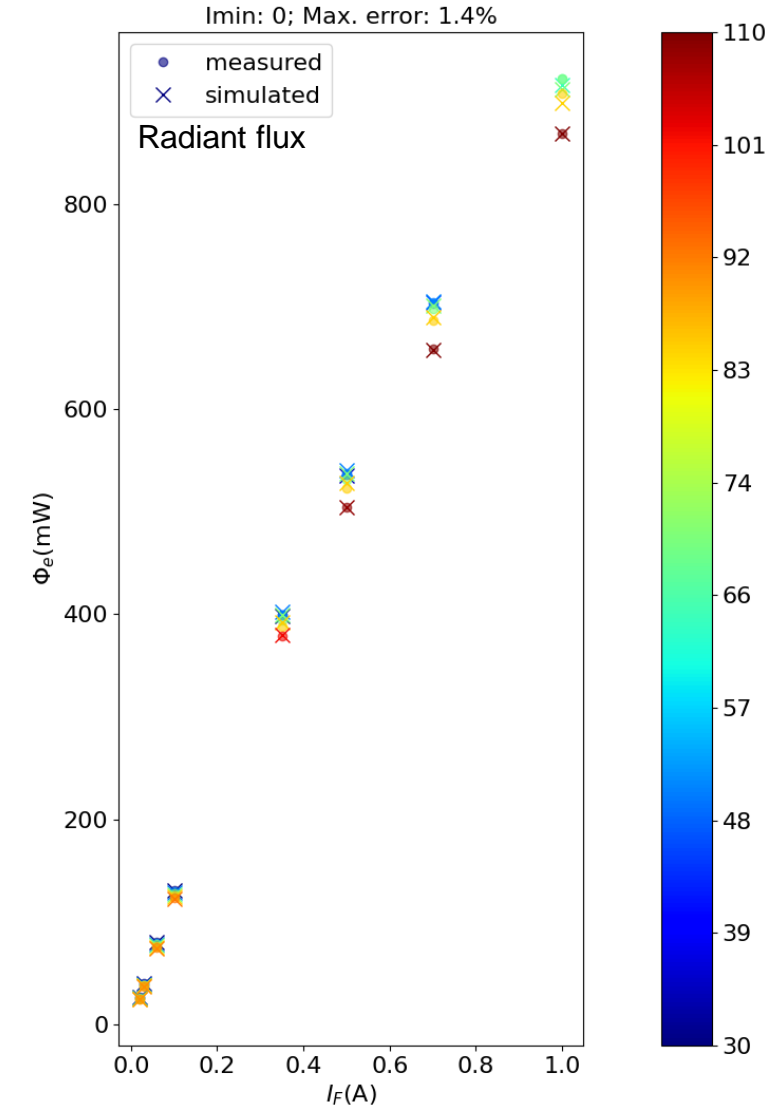
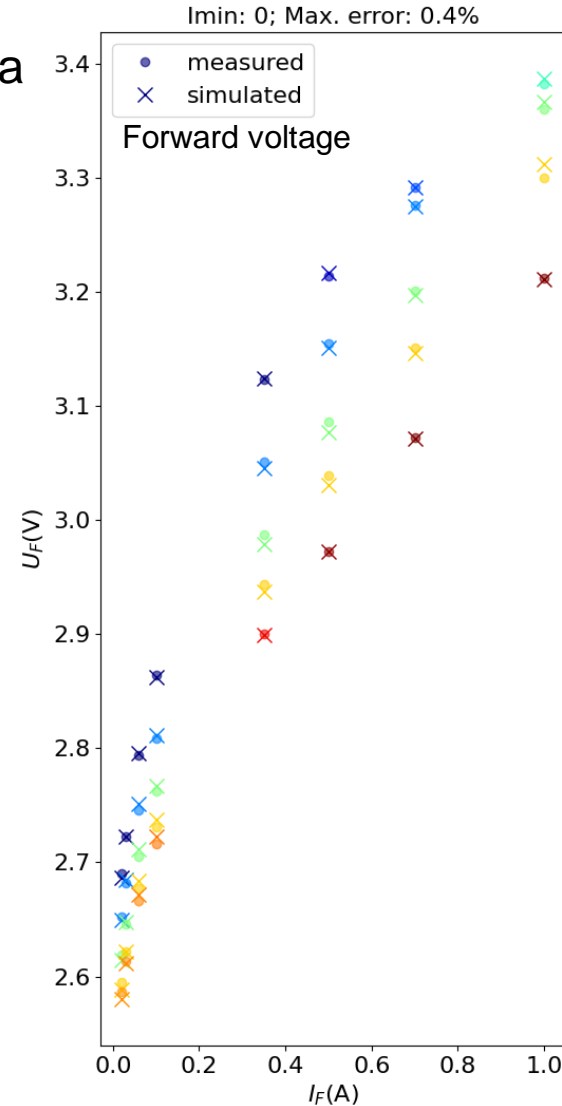
- The extraction was tested on all Delphi4LED measurements, which are available; including both white and colour LEDs
- The relative error of the modelled radiant flux for the whole was below 5%.
  - This is the same order of magnitude as the measurement uncertainty of the radiant flux)
- The relative error for the forward voltage was below 1%.
- The execution time for parameter extraction from **40 operating points was less than 1 minute**

$$V_{F,T_j=T_{ref}} = I_F \cdot R_S + m \cdot U_T \cdot \ln \left[ \left( \frac{I_F}{I_0} \right) + 1 \right]$$

$$\Delta V_{F_{el}} = (a_{el} \cdot I_F^2 + b_{el} \cdot I_F + c_{el}) \cdot (T_j^2 - T_{ref}^2) + (d_{el} \cdot I_F^2 + e_{el} \cdot I_F + f_{el}) \cdot (T_j - T_{ref})$$

$$I_{rad}(V_{Frad}) = I_{0rad} \cdot \left[ \exp \left( \frac{V_{Frad} - \Delta V_{Frad} - I_{rad} \cdot R_R}{m_{rad} \cdot U_T} \right) - 1 \right]$$

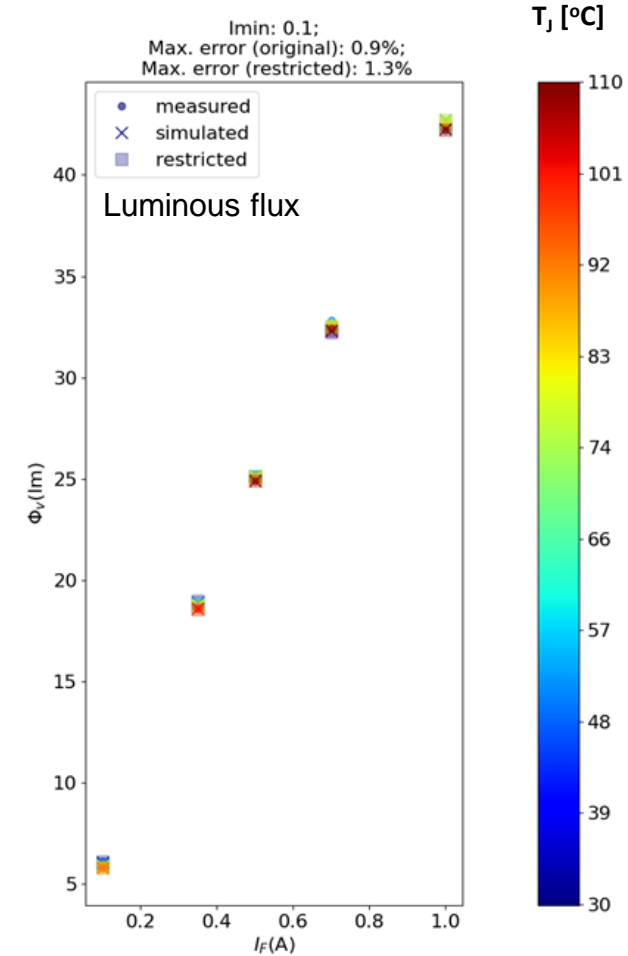
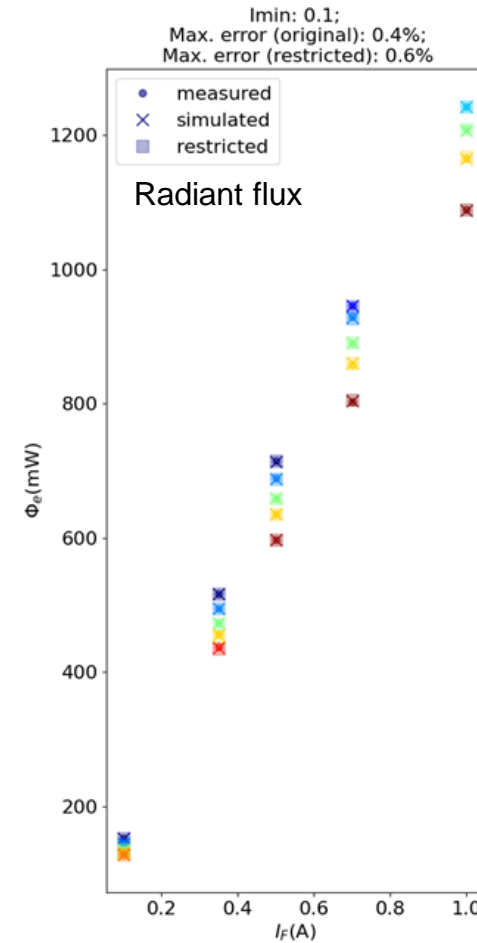
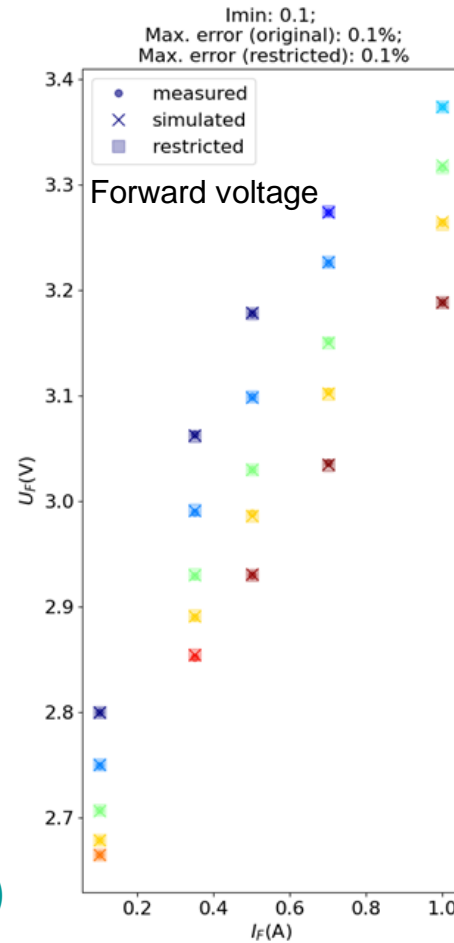
$$\Delta V_{Frad} = (a_{rad} \cdot I_F^2 + b_{rad} \cdot I_F + c_{rad}) \cdot (T_j^2 - T_{ref}^2) + (d_{rad} \cdot I_F^2 + e_{rad} \cdot I_F + f_{rad}) \cdot (T_j - T_{ref})$$



# Some steps taken forward: parameter extraction for the chip level multi-domain model

Reduce the number of necessary ( $I_F$ ,  $T_J$ ) operating points of Delphi4LED measurements:

- It seems that measuring at 3 temperatures and 4 currents (12 operating points instead of 40) results in less than 1% additional error in the model.
- A more detailed analysis is in progress that compares the data from 170 operating points reduced down to 12-15 ones.
- **The measurement time can be halved without significant errors in the results: additional benefit on top of developments aimed at speeding up tests (isothermal IVL characterization)**



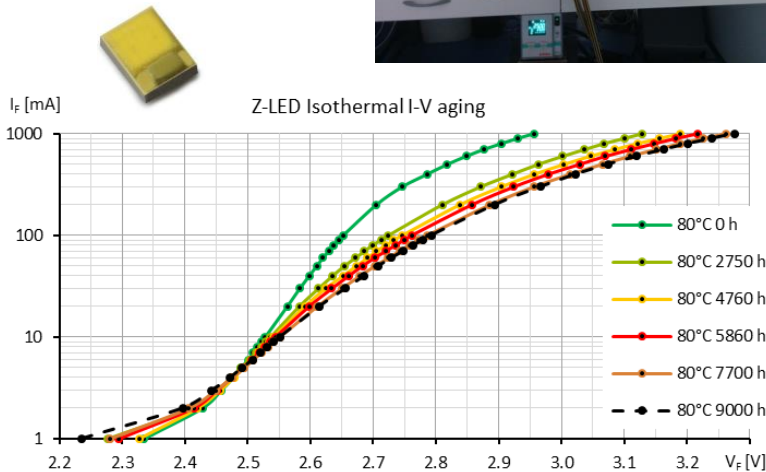
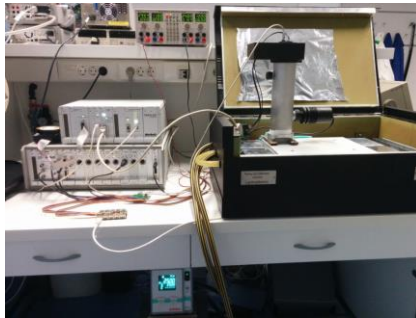
# Elapsed lifetime – age dependence of model parameters

From past ageing measurements

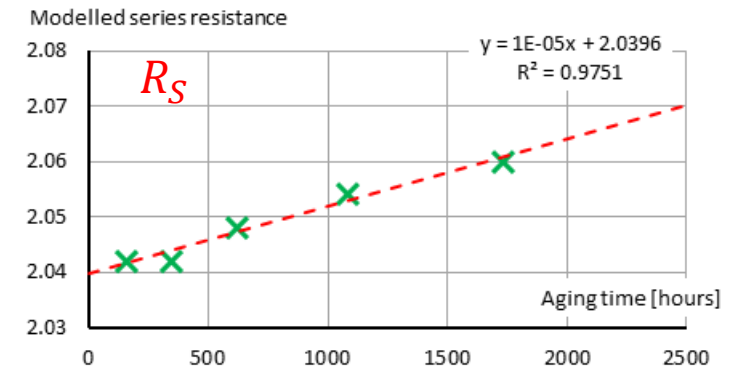
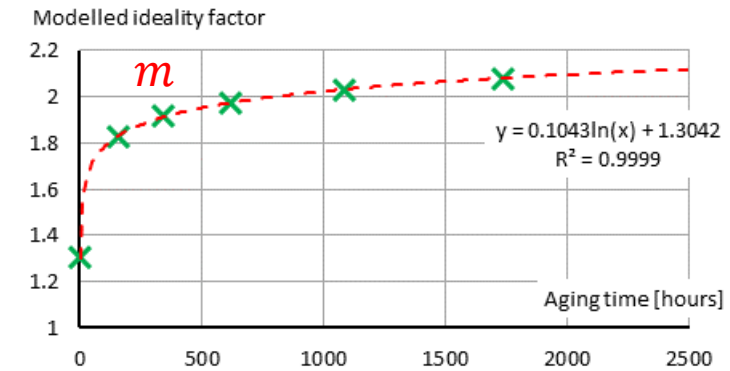
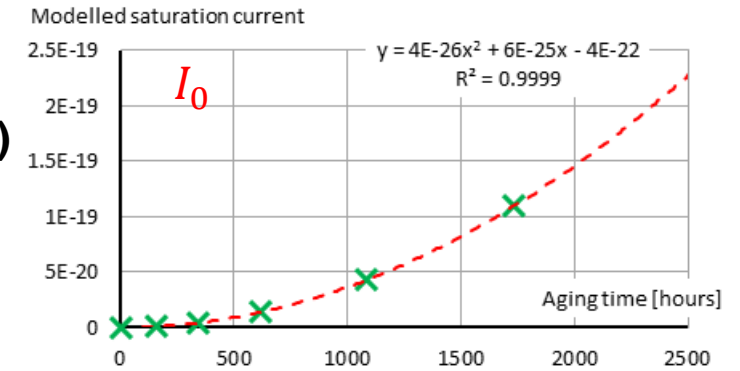
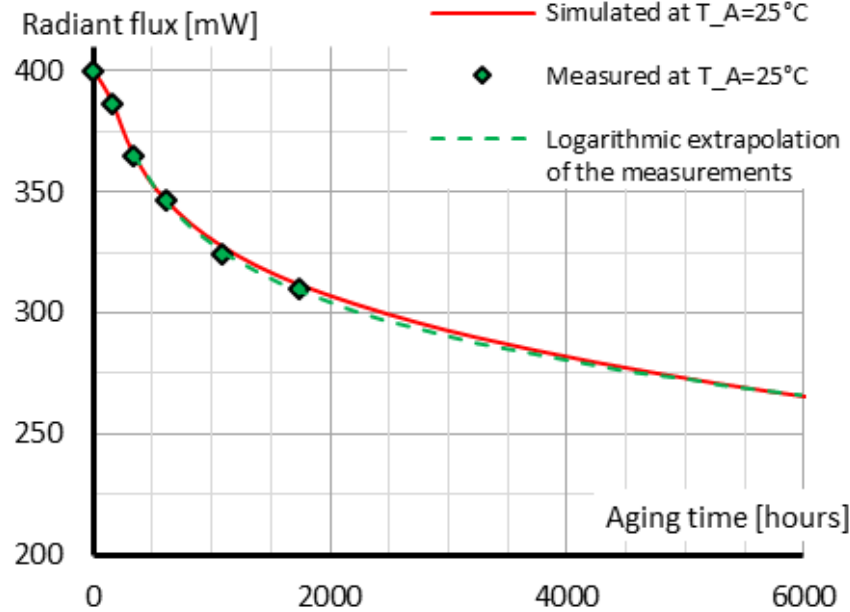
- **Elapsed lifetime in the multi-domain LED model (fixed current and temperature)**
  - 100% ... 78% aging range (in terms  $\Phi_V$ )
- **Successful implementation of this very first approach – fitting LM80 test data**
  - 0.5% absolute and
  - 1.2% maximum simulation inaccuracy

$$V_{F,T_J=T_{ref}} = I_F \cdot R_S + m \cdot U_T \cdot \ln \left[ \left( \frac{I_F}{I_0} \right) + 1 \right]$$

LM80 aging test setup completed with equipment for isothermal IVL characterization at an academic partner



Isothermally measured IV characteristics obtained at different aging times during an LM80 test

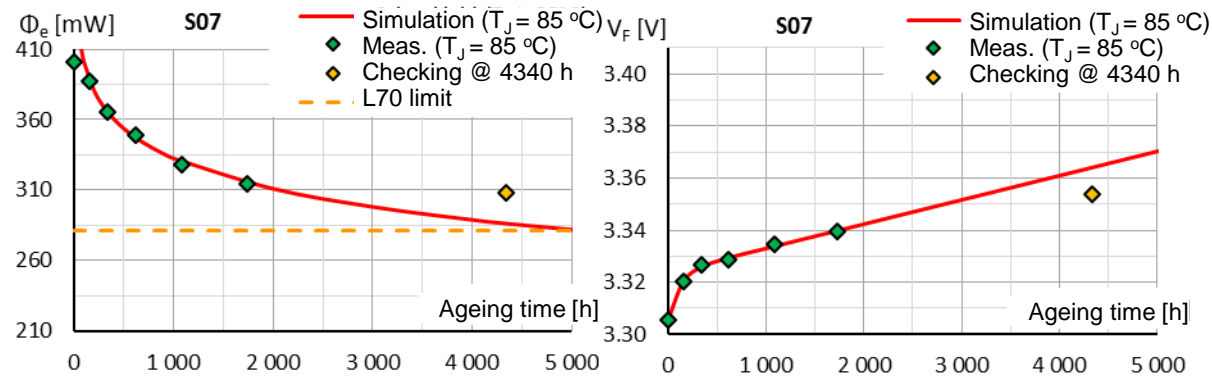


# Elapsed lifetime – as an additional parameter of the Spice-like multi-domain model

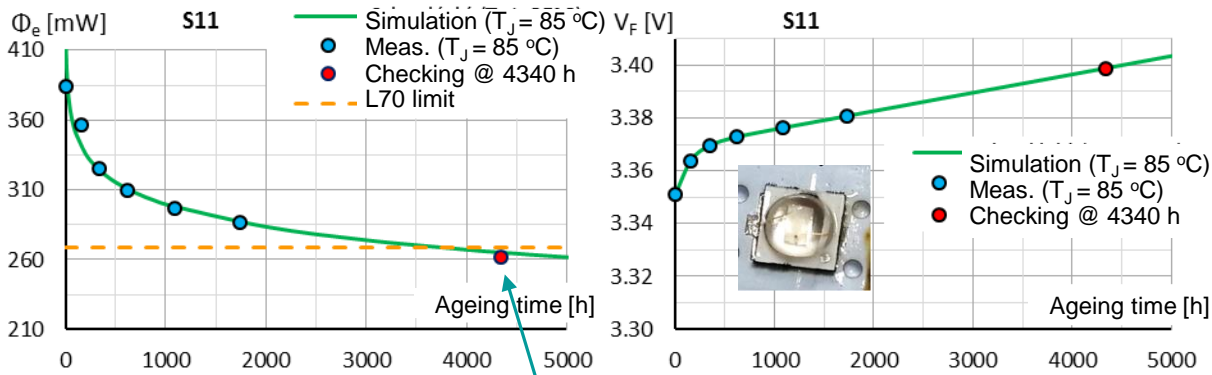
From previous LM80 aging test of another set of samples

- models were generated from data measured up to 1735 hours,
- after further ageing up to 4340 hours, the samples were measured again.

The model predicted flux depreciation and the measured one matched well.



	$V_F$ error of modelling [mV]	$V_F$ error related to the zero hour value [%]	$\Phi_e$ error of modelling [mW]	$\Phi_e$ error related to the zero hour value [%]
S07	10.2 mV	0.3%	-21.7 mW	5.4%
S11	0.1 mV	0.003%	3.2 mW	0.8%



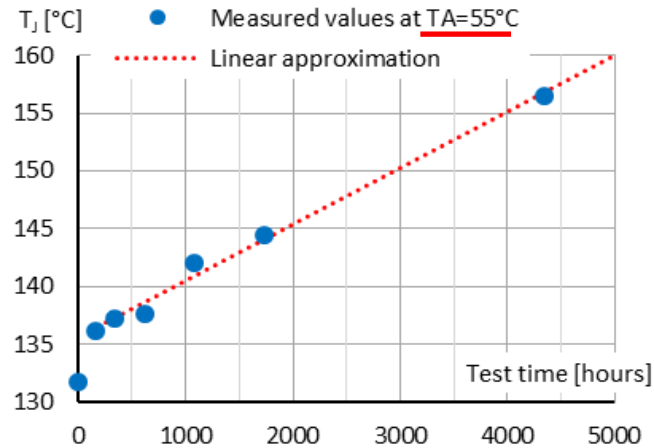
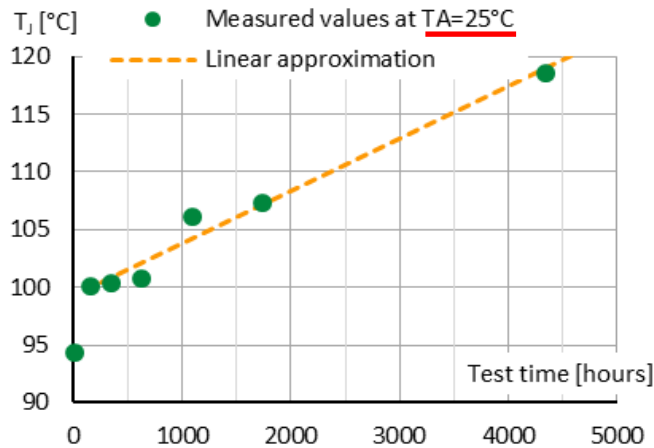
Poor product, L70 end-of-life reached in ~4300 hours.

## Problems:

- Too few samples were studied
- LM80 aging test + isothermal IVL characterization in 40 operating points takes impedingly lot of effort
- Only one aging current and aging temperature was used

## Some measurement issues need also be clarified...

During LM80 tests continuous increase of the junction temperature was observed (BME's experiments)



In the TM21 based life-time estimation the constant ambient temperature is used...

At least for chip level ageing, the junction temperature counts, though.

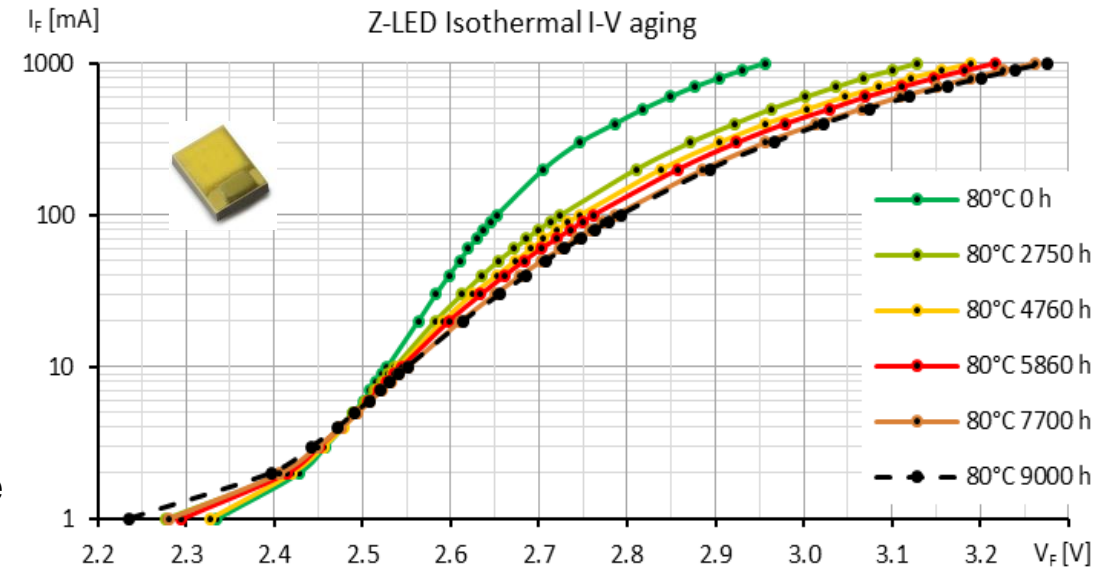
What if, we are interested in the predicted life-time at

- another constant forward current,
  - at another temperature,
  - or both?
- } → mission profile

### LM80 tests:

**Conditions:** LEDs driven by a constant DC current in a constant temperature (e.g. 55 °C, 85 °C) environment.

**Aging indicator:** maintenance of the emitted total luminous flux

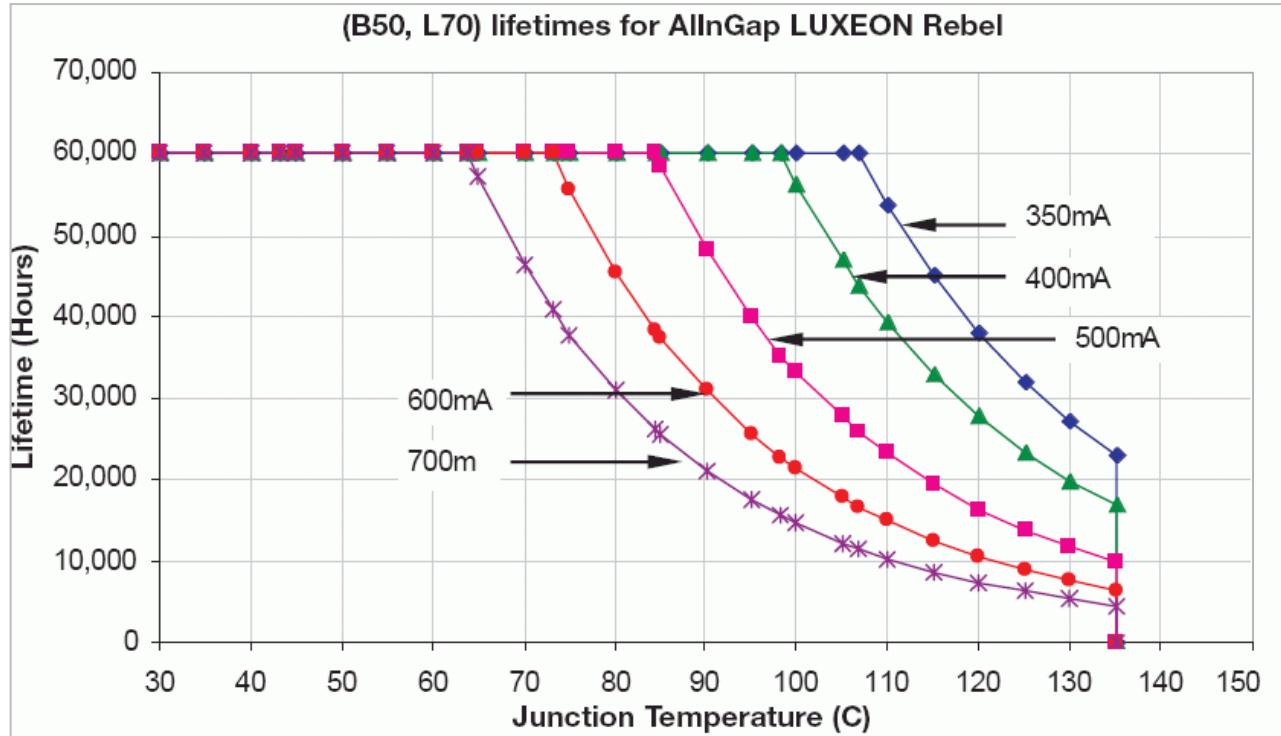


### TM21 life-time prediction:

Fitting an Arrhenius-type relationship to the LM80 luminous flux maintenance data

# Why is the mission profile interesting?

Both higher forward current and higher temperature speed up LED ageing



Changing  $I_F$  and  $T_J$  are due to changes

- as part of **normal operation**,
- and due to **changing environment** (weather)

often superimposed, resulting e.g. in

- short term **active cycles** (dimming, on/off cycles)
- daily and seasonal **passive cycles**.

**mission profile**

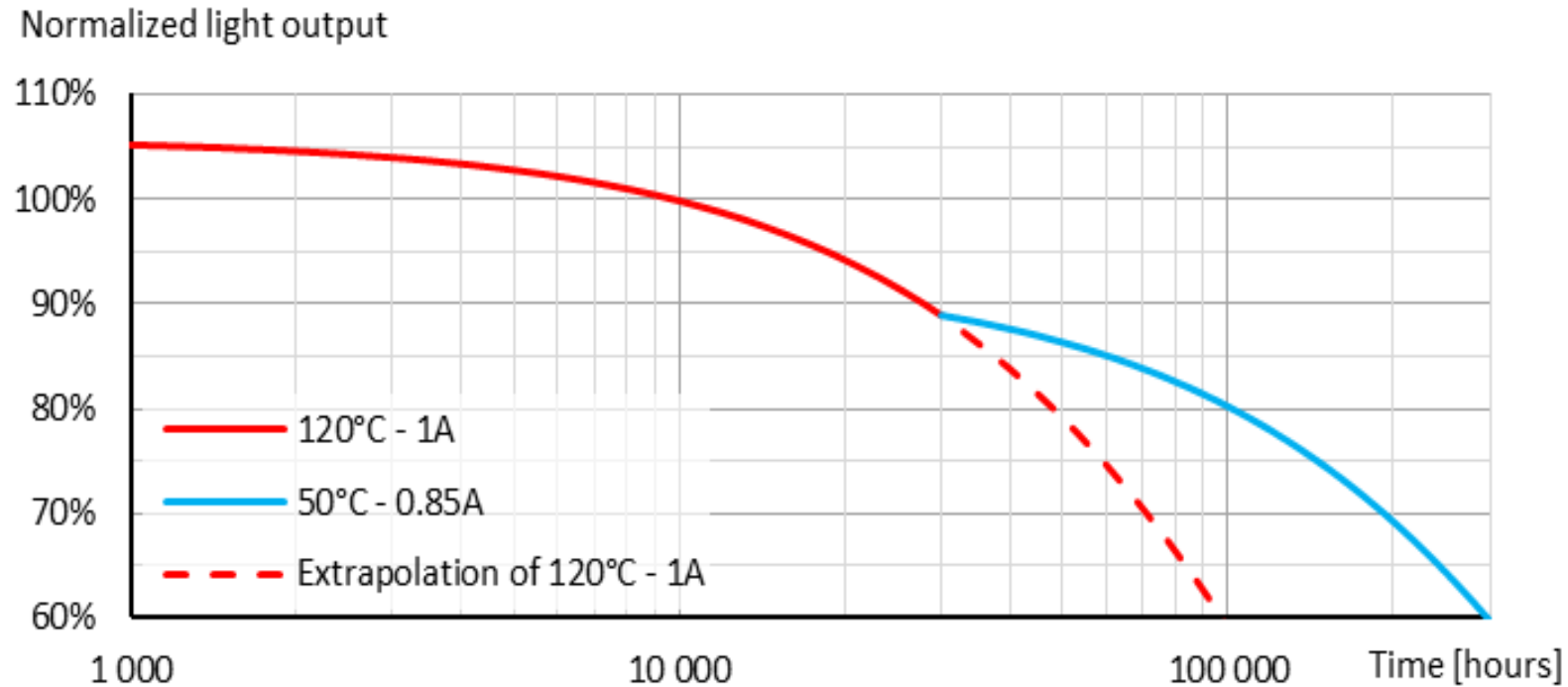
Besides e.g. chip level ageing, **thermo-mechanical stresses** develop, resulting in degradation of the heat-flow path → **increased  $R_{th}$**  → **increased  $T_J$**

## Hypothesis:

- There is a “**life-time budget**” identified through an LM80 aging process (given  $I_F$  and  $T_J$ ) and TM21 prediction.
- **This budget is consumed faster or slower with changing  $I_F$  and  $T_J$**
- Acceleration can be **calculated also with an Arrhenius-type relationship** (analogy with the description of kinetics of chemical reactions)

# The effect of "mission profile" on the LM80/TM21 luminous flux maintenance curve

At L90 temperature and current are reduced – projected L70 life-time got prolonged:



Degradation dynamics (**data-based part**)

$$\dot{x}(t) = f(x(t), u(t)), \quad x(0) = x_0$$

Effects of degradation dynamics on the LED chips' optical output

$$\Phi_V(t) = g(x(t), u(t), \theta)$$

$x(t)$ : the state of degradation,  $0 < x < 1$

$g(1, u, \theta)$ : the multi-domain LED model

$\theta$ : parameters of the multi-domain model

$u$ : vector of operating conditions (current, temperature, etc) – the "mission profile"

$\Phi_V(t)$ : luminous flux

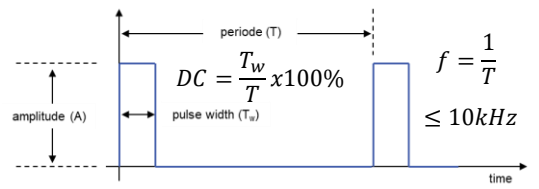


# Considering the ageing effect of cyclic electro-mechanical stresses

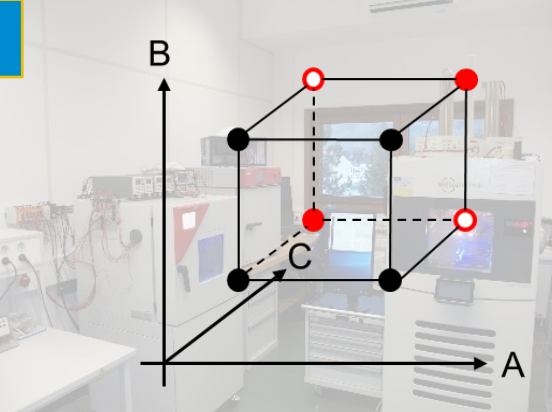
In relation this we can learn again a lot from the practice of the semiconductor industry...

LM80

+ Power Cycling (Duty Cycle)



+ DoE



Collect Knowledge + Data

- System Understanding
- Fault types, States
- Measurements

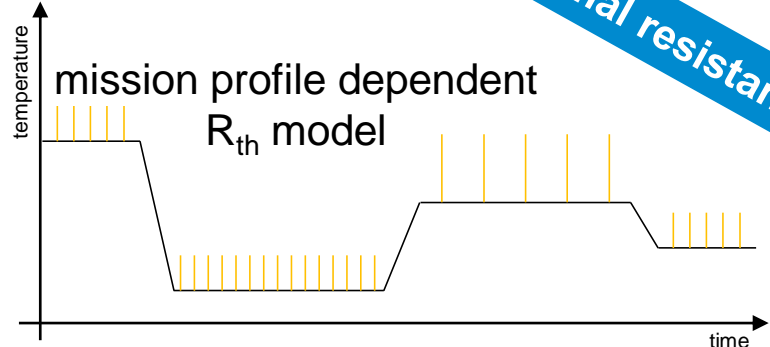
Modelling changes of thermal resistance due to ageing

Construct inverse model family

- Exploratory Data Analysis
- Analytical inverse model
- Data-driven inverse model

Explore inverse model family

- Trade-off studies
- Uncertainty quantification
- Model complexity

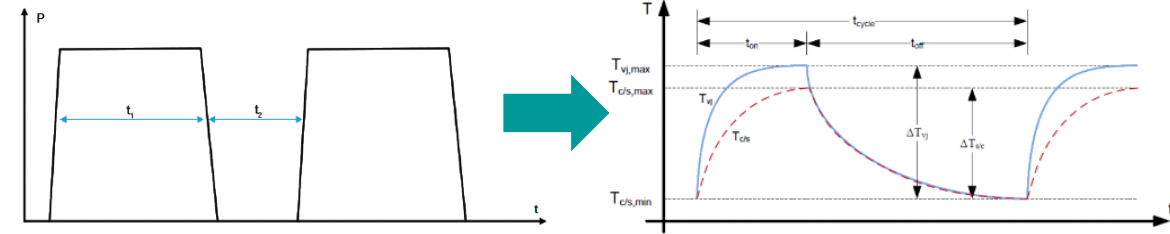


Slide by courtesy of Julien Magnien, MCL, Leoben, Austria

# Learning from electronics again: power cycling of power semiconductor devices (IGBTs)

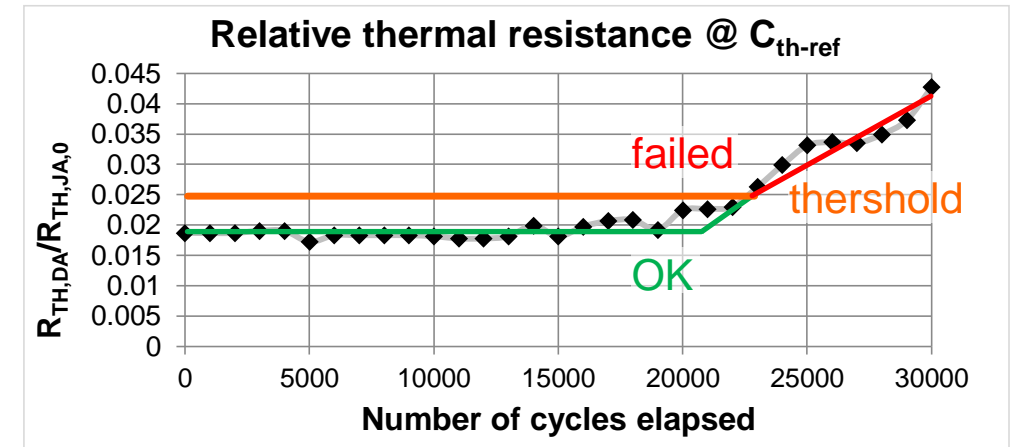
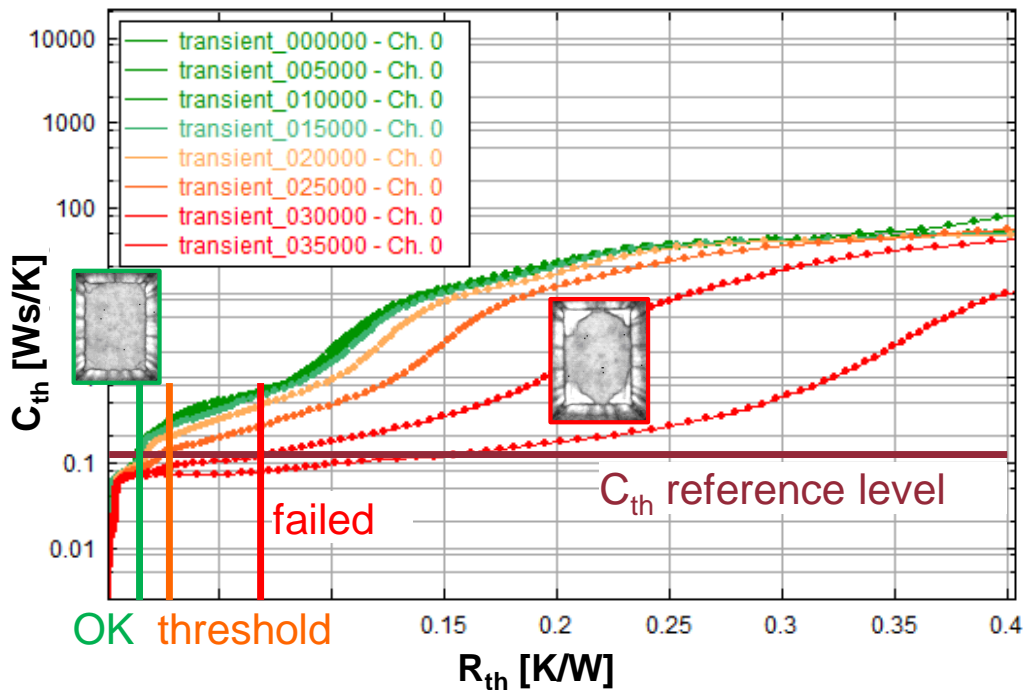
## Life-time assessment of a power semiconductor device after cyclic stress

- Find the location and degree of degradation
- Early detection of future failures before fatal failure of the device
- *In-situ*, non-destructive method, applicable during field operation



## A failure mode also possible in LED packages: die attach degradation/delamination

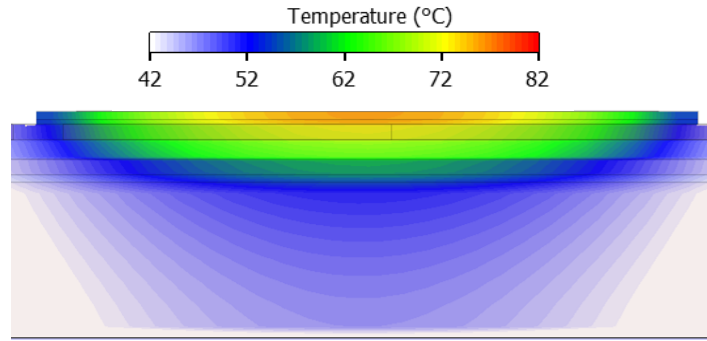
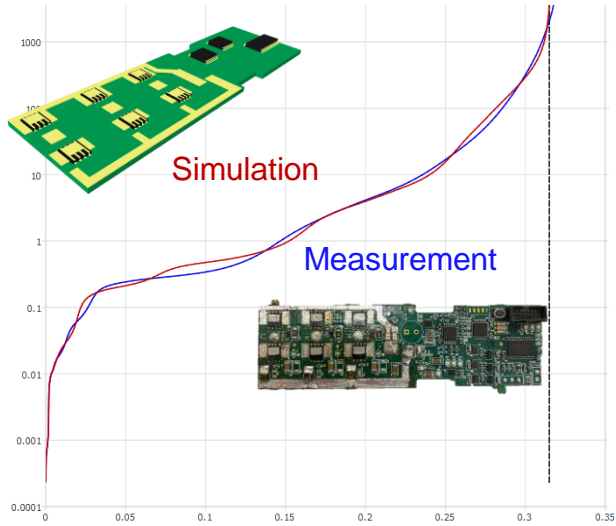
### Structure functions after different numbers of elapsed cycles



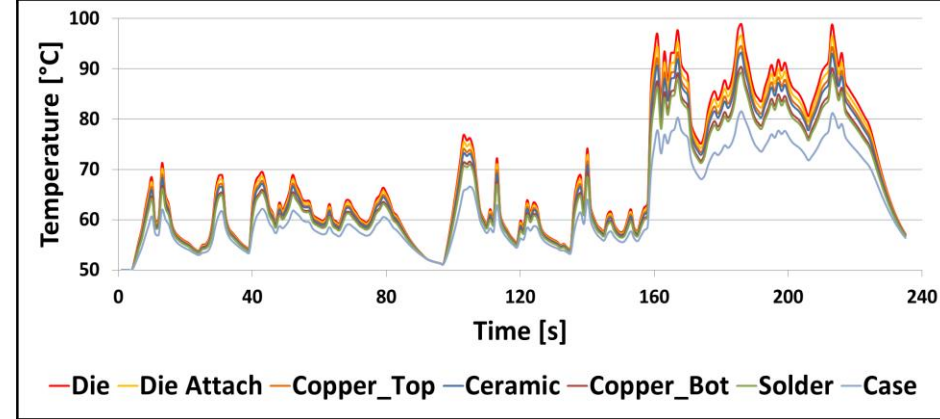
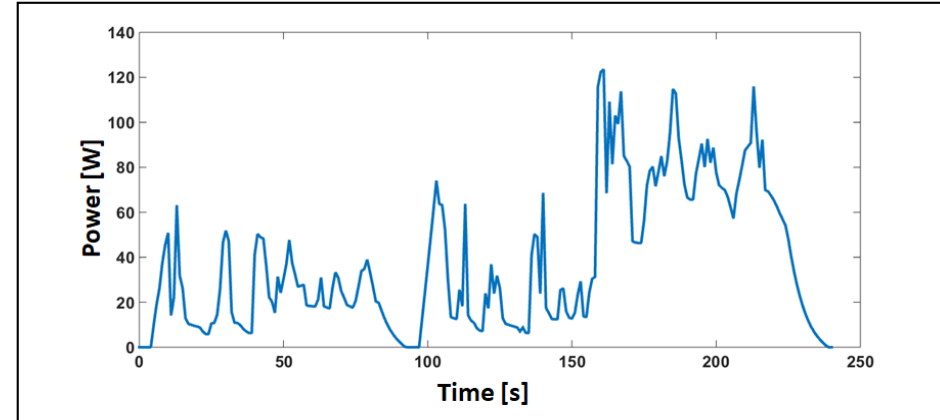
**Failure condition:** intersection of the structure function and a  $C_{th} = C_{th/ref}$  reference level is beyond an  $R_{th}$  threshold.

*The question is how many cycles are needed to reach it...*

# Life-time assessment of a power semiconductor device after cyclic stress

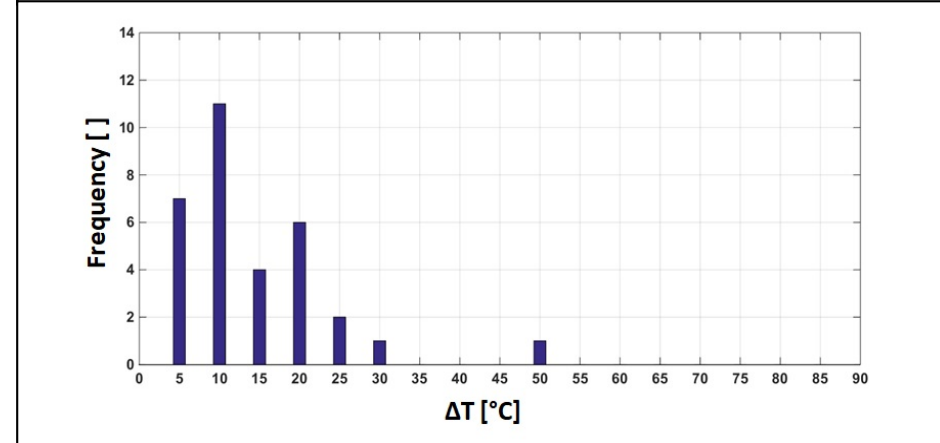
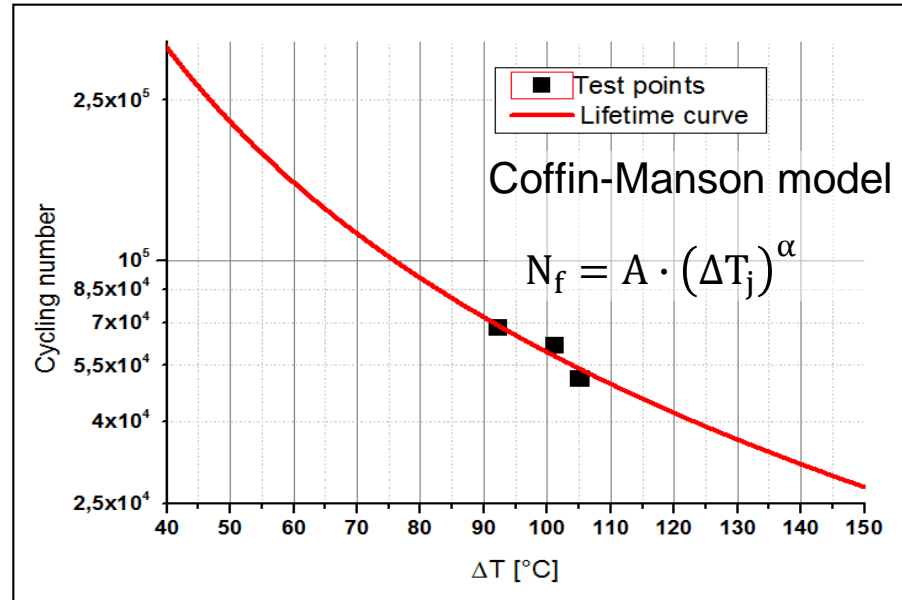


Calibrated detailed 3D model  
(ROM based compact model would also work)



$$N_{f\_sum} = \frac{1}{\sum_{k=1}^n \frac{w_i}{N_{f,i}}}$$

$$t_{operation} = N_{f\_sum} \cdot t_{cycle}$$



# Example: self-learning digital twin assisted age and temperature compensated CLO

- A Delphi4LED digital twin application example was a temperature compensated CLO scheme in a street-lighting luminaire.
- It relied on a multi-domain LED model valid at 0 h
- Its benefits were
  - Overlighting was avoided at low temperatures (winter) by reducing the forward current
  - According to model calculations and [archived met data for Hungary](#), this solution may result in the [reduction of the necessary electric power of about 5-8%](#)

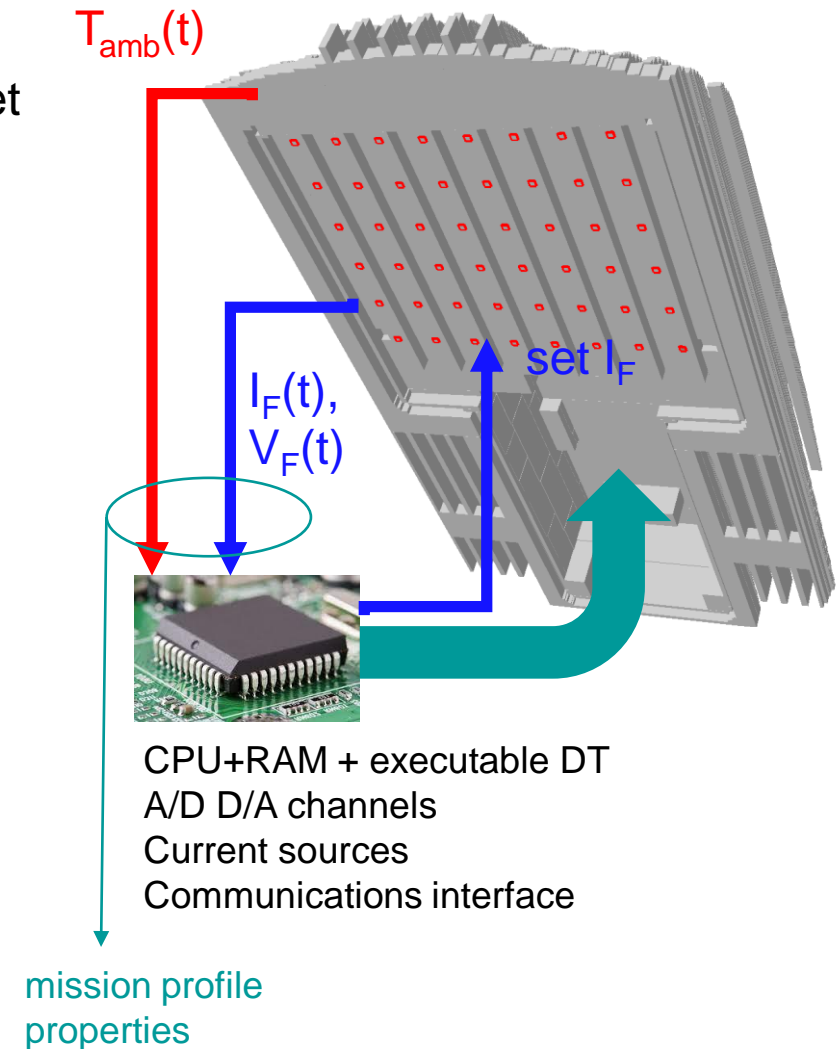
## Why to deal with ageing in a CLO scheme?

- The required illumination level has to be provided even when the product is close to the L70 condition (luminous flux shrank to 70% of its initial value)
- This could be achieved by increasing the forward current as the LEDs get aged.
  - For a precise setting of the forward current, instead of the standard LM80/TM21 luminous flux maintenance, the actual elapsed mission profile based luminous flux maintenance function should be considered
  - The self-learning feature in this case means the continuous update of the consumed life-time budget

## Life-long constant light output control: a street-lighting luminaire example (cont.)

### Self-learning feature, remaining useful life-time (RUL) prediction

- The self-learning == continuous update of the consumed life-time budget according to the mission profile measured
- This requires the following features in the luminaire
  - Some monitoring / diagnostic features such as
    - measurement of the luminaire/ambient temperature
    - measurement of diode voltages
    - measurement of other parameters like RH, color, etc.
  - Fine resolution in the setting of the forward current in the LED driver
  - Data processing capabilities in the LED driver
    - hosting the executable digital twin (age-extended multi-domain LED model)



As an application use-case, the previously presented temperature compensated CLO scheme is planned to be extended with such an SLDT (self-learning digital twin) in AI-TWILIGHT

## Some *expected* quantified benefits of ageing compensated CLO using an SLDT

The below table is based on the properties of a white LED aged a few years ago at BME and on temperatures from archived met data (Szombathely, NW Hungary)

	No CLO (constant current during life-time)	CLO with temperature and ageing compensation	Benefits of using the SLDT assisted CLO
Projected life- time until L90 condition	64.4 khours	83 khours	+29%
	16.7 years	21.4 years	+4,7 years
Power consumption during 64.4 khours	130.8 kWh	112.8 kWh	-13.7%
Power consumption in the first year	7.9 kWh	6.5 kWh	-17.7%

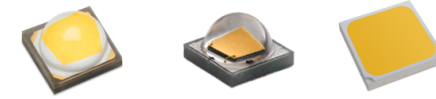
# | Where AI can help...



# Where is AI support expected?

## Help model (parameter) extraction from physical test results

- The concept of "carrier devices": an LED vendor agnostic approach
  - Catalog of different LED devices representative in a given application domain established (multiple classes of similar architectures)
  - A few devices will be fully characterized (isothermal IVL characteristics in multiple operating points)
  - These will be a training set for an AI that is aimed at producing model parameter sets of other devices of the same architecture



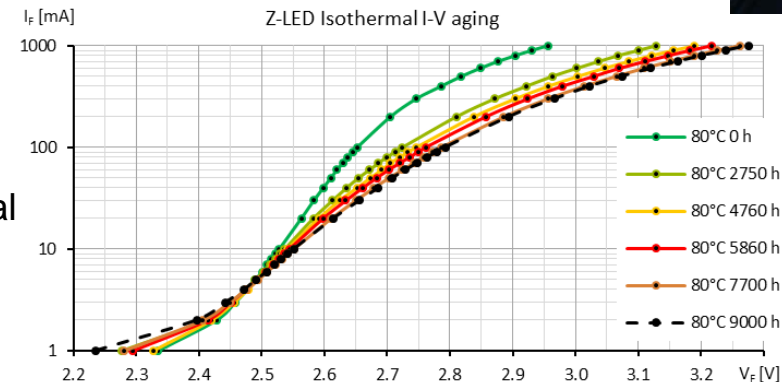
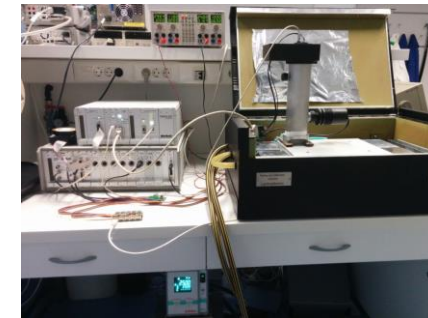
Category	PSS-FC based HP	HP VTF based HP	Multi-die single emitter
Example product models	LUXEON HL2X Cree XP-G3 Nichia 219C Samsung LH351C	Cree XP-G2 Osilon Square	LUXEON 5050 SSC 5050 Duris S8
Package type	Ceramic	Ceramic	Lead frame
Die type	PSS-FC	VTF	Lateral
Die area (mm <sup>2</sup> )	2	2	
Die wavelength (nm)	440-460	440-460	440-460
CCT (K)	2700 4000	4000	4000
CRI	70	70	70

Some carrier devices for outdoor applications

## Help using archive sets of data (the AI-TWILIGHT database)

- Large amount of **industrial test data** (qualification test data, LM80 life-time test data), **Deelphi4LED datasets**, detailed isothermal IVL data sets obtained during LM80 ageing for a few LEDs from **academic experiments**
  - The detailed academic test data sets and their corresponding industrial counterparts will be a training set for an AI aimed at generating parameter sets for LEDs for which only the industrial data sets are available

LM80 aging test setup completed with equipment for isothermal IVL characterization at an academic partner

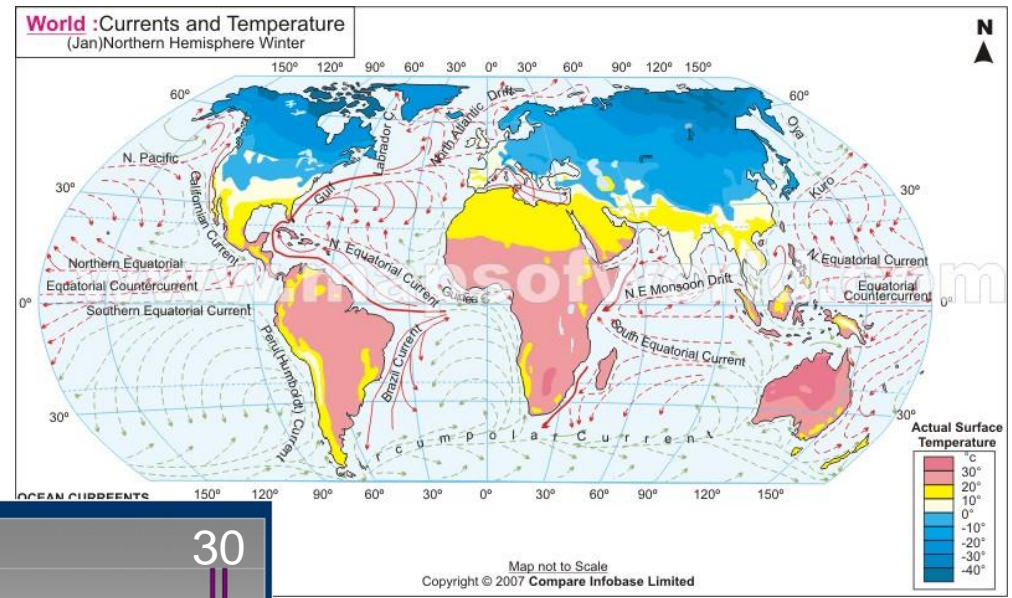


Isothermally measured IV characteristics obtained at different aging times during an LM80 test

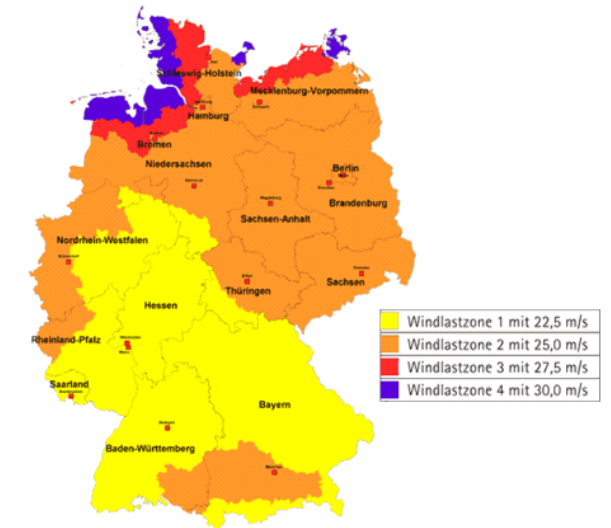
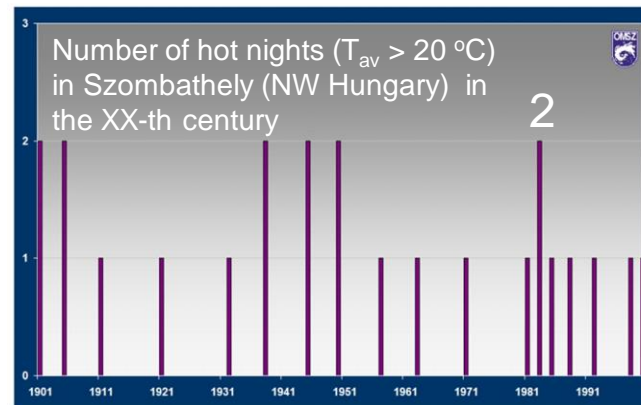
# Where is AI support expected?

## Help connect test data from the field with lab test data

- There are luminaires in the field equipped with different diagnostic capabilities and sensors
- Historical data sets are available from such sources
  - Temperature data (ambient, luminaire, solder point, etc.)
  - Forward voltage data (that can be related to  $T_j$ )
- From the above data find actual “mission profiles” of luminaires resulting from
  - the operation (on/off cycles) and
  - the environmental conditions (ambient temperature variations)
- Such luminaires can be brought back to the lab to be tested in details



Global world temperature distribution in January



Average wind speed distribution in Germany

# The team behind this:

**DE**  
HELLA, SIMSCALE, BMW, JCMwave, TECHNISCHE UNIVERSITÄT DARMSTADT

**NL**  
TU Delft, TU/e EINDHOVEN UNIVERSITY OF TECHNOLOGY, signify, LUMILEDS

**FR**  
ingélux Consultants, Eccelectro LED innovation, GROUPE arcom Smart building & smart city, citeos

**IT**  
infineon, UNIVERSITÀ DEGLI STUDI DI PADOVA

**PL**  
GL OPTIC Light quality control

**HU**  
MŰEGYETEM 1782, HUNGAROLUXLIGHT, FAKT Hungaria, Lighting lab

**AT**  
mC, TRIDONIC, MEDS

**CH**  
Pi Lighting



**AI-TWILIGHT**  
[www.ai-twilight.eu](http://www.ai-twilight.eu)

24 partners from 8 European countries

**AI-TWILIGHT: AI powered Digital twin for lighting infrastructure in the context of front-end Industry 4.0**



# The team behind this:



	AT	CH	DE	FR	HU	IT	NL	PL
<b>Major companies</b>	TRIDONIC		HELLA BMW	citeos		Infineon	signify LUMILEDS	
<b>Academia</b>	mcl		TECHNISCHE UNIVERSITÄT DARMSTADT		MŰEGYETEM 1782	UNIVERSITÀ DEGLI STUDI DI PADOVA	TU Delft TU/e Eindhoven University of Technology	
<b>SMEs</b>	MEDS	Pi Lighting	SIMSCALE JCMwave	ingélux Consultants Ecclectro LED innovation	Lighting Lab FAKT Hungaria HUNGAROLUXLIGHT		GL OPTIC	

## AI-TWILIGHT: AI powered Digital twin for lighting infrastructure in the context of front-end Industry 4.0



# Open access papers on some of the addressed topics

<https://doi.org/10.3390/en12101909>  
<https://doi.org/10.3390/en12122389>  
<https://doi.org/10.3390/en12091628>  
<https://doi.org/10.3390/en13184979>  
<https://doi.org/10.3390/en13133370>

The screenshot displays a web browser window with multiple tabs open, all pointing to MDPI articles. The active tab shows the article page for 'Lifetime Modelling Issues of Power Light Emitting Diodes' in the journal 'Energies'. The page includes a search bar, article metadata, author information, and an abstract. The MDPI logo is visible at the top left of the page content.

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## Lifetime Modelling Issues of Power Light Emitting Diodes

by János Hegedűs, Gusztáv Hantos and András Poppe

Department of Electron Devices, Budapest University of Technology and Economics, 1117 Budapest, Hungary  
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(This article belongs to the Special Issue Thermal and Electro-thermal System Simulation 2020)

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### Abstract

The advantages of light emitting diodes (LEDs) over previous light sources and their continuous spread in lighting applications is now indisputable. Still, proper modelling of their lifespan offers additional design possibilities, enhanced reliability, and additional energy-saving opportunities. Accurate and rapid multi-physics system level simulations could be performed in Spice compatible environments, revealing the optical, electrical and even the thermal operating parameters, provided, that the compact thermal model of the prevailing luminaire and the appropriate elapsed lifetime dependent multi-domain models of the applied LEDs are available. The work described in this article takes steps in this direction in by extending an existing multi-domain LED model in order to simulate the major effect of the elapsed operating time of LEDs used. Our approach is based on the LM-80-08 testing method, supplemented by additional specific thermal measurements. A detailed description of the TM-21-11 type extrapolation method is provided in this paper along with an extensive overview of the possible aging models that could be used for practice-oriented LED lifetime estimations. View Full-Text

## Acknowledgments

Part of the activities behind this work were partially supported by the AI-TWILIGHT H2020 ECSEL project through the grant agreement H2020 ECSEL RIA 101007319 of the EU and the grant agreement 2019-2.1.3-NEMZ\_ECSEL-2021-00008 of the Hungarian National Research and Development Fund



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